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BLAST EFFECTS OF SIMULTANEOUS MULTIPLE-CHARGE DETONATIONS

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BEFORE COMPLETING FORM REPORT DOCUMENTATION PAGE 2. GOVT ACCESSION NO. 3. RECIPIENT'S CATALOG NUMBER Contractor Report ARLCD-CR-78032 TITLE COUNT SUBSCILLAN BLAST EFFECTS OF SIMULTANEOUS MULTIPLE-CHARGE DETONATIONS. PERFORMING ONG. REPORT NUMBER CONTRACT OR GRANT NUMBER(+) J.C. Hokanson, E.D. Esparza, A.B. Wenzel Swall P.D. Prices ARMADOOM Project Loader PERFORMING ORGANIZATION NAME AND ADDRESS Southwest Research Institute -P.O. Drawer 28510 San Antonio, Texas 78284 1. CONTROLLING OFFICE NAME AND ADDRESS US Army ARRADCOM OCTOBER 1978 ATTN: DRDAR-TSS Dover, NJ 07801 115 14 MONITORING AGENCY NAME & ADDRESSIS different from Controlling Office) SECURITY CLASS. (of this report) US Army ARRADCOM Unclassified ATTN: DRDAR-LCM-SP SA. DECLASSIFICATION DOWNGRADING Dover, NJ 07801 16. DISTRIBUTION STATEMENT (of this Report) Approved for public release; distribution unlimited 18. SUPPLEMENTARY NOTES JAN 22 1979 19. KEY WORLDS (Continue on reverse side if necessary and identify by block number) В Blast Measurements Impulse Simultaneous Detonation Duration Explosives Time of Arrival Prossure 20. ABSTRACT (Continue on reverse side if necessary and identify by black number) This report describes an experimental program conducted by Southwest Research Institute in support of the Army Plant Modernization Program. Air blast parameters including peak pressure and specific impulse were measured for multiple charges, A detonated simultaneously, in three different geometrical configurations: grouped, horizontal and vertical arrays. A series of single charge tests was also conducted to establish a bascline from which the

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20. ABSTRACT (Cont'd)

effects of multiple charges could be determined. A model analysis was developed and used to design and interpret the model experiments.

In the experiments, pentolite spheres modeling potential explosive sources were detonated near a reflecting surface. Blast measurements were made directly below the charges and at various slant distances using piezoelectric transducers. The impulse was obtained by numerically integrating the pressure traces. Plots of peak pressure, impulse, duration and arrival time are presented and the differences between single and multiple Charges are highlighted.

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INTRODUCTION

This report describes an experimental program conducted by Southwest Research Institute (SwRI) for the U.S. Army Armament R & D Command, Dover, New Jersey under Contract Number DAAA21-76-C-0254. As part of the Army Plant Modernization Program, air blast parameters have been measured in the past for single explosive sources, and propellents and pyrotechnics in their in-process and final product forms.

In a plant process there are often multiple explosive sources within a single room, on a conveyor or near a barricade. Currently, structures which may be loaded by simultaneous or near simultaneous multiple detonations are designed according to Section 4-17 of Reference 1. According to this document, the impulse loading on the structure is approximated by the numerical sum of the impulse which would be generated by each individual explosion whenever the combined duration is less than 1/3 of the response time of the structure. For combined durations longer than 1/3 the structure response time, the actual pressure-time history should be replaced by a fictitious peaked triangular pulse similar to that for a single explosion. The objective of this program is to investigate blast phenomena near a reflective surface due to multiple simultaneous detonations at small scaled distances This information will be used to supplement the information contained in Reference 1. Eventually, it is hoped that this information will lead to a more realistic design of buildings used for the manufacture of explosives and propellents.

In this program, the blast parameters of several charge geometries were measured at different charge spacings and standoff distances. At large distances, the shock fronts from several charges detonated simultaneously should coalesce and be more or less indistinguishable from that of a single charge with an equivalent amount of explosive. To ensure that measurements were made before the individual shock fronts had begun to coalesce, the transducers were placed at small scaled distances ($Z \le 1.2 \text{ m/kg}^{1/3}$ or $3.0 \text{ ft/lb}^{1/3}$). Since this was an exploratory program, the tests were organized in the following manner.

- . The number of charges was held constant at three,
- . All three charges were detonated simultaneously,
- . The in-process explosive sources were simulated with Composition B spheres.
- . Three charge geometries were investigated: Grouped, Horizontal and Vertical Arrays.
- The spacing between charges in the horizontal and vertical array tests was uniform.

The blast parameters measured included peak pressure, specific impulse, positive duration and time of arrival. The pressure-time traces were recorded with piezcelectric transducers and the impulse was obtained by integrating the pressure histories.

A total of 44 tests was conducted in four test geometries. Nine transducers were placed at regular intervals in a straight line. The test charges were suspended above a reflective surface at scaled distances ranging from 0.335 m/kg $^{1/3}$ (0.84 ft/1b $^{1/3}$) to 1.18 m/kg $^{1/3}$ (3.0 ft/1b $^{1/3}$). Each charge was initiated with an exploding bridgewire detonator. A series of single charge tests was used to establish a baseline from which the relative blast output of multiple versus single charges could be determined. This series of tests was also used to check out the instrumentation system, for calibration and to validate the model analysis. A series of tests in which three charges were grouped together was conducted. These tests were designed to determine whether charges packed together behave the same as a single charge of equivalent weight. The horizontal array tests may be thought of as simulating a conveyor system or explosive sources distributed horizontally. Charge spacing and standoff distance were varied in these tests. Of particular interest in the horizontal array tests was the poss(bility of regions of enhanced pressure and impulse between the charges. The final tests were conducted to determine the blast output of charges suspended above the ground in a vertical array.

In this report a technical discussion is given in which the model law is developed. The model law was used to design the experiments and interpret the data. The section entitled Experimental Program outlines the test program, the instrumentation used to measure the blast parameters and the data reduction methods. The resulting data are presented principally in the form of graphs. Comparison of the blast output of single and multiple charges is made, and tables of all the test data are included as an Appendix to this report.

General

The blast output from the detonation of a single explosive source in the free field has been well defined for many years. A complete description of the blast output is found in Reference 2. To better describe the characteristics of the simultaneous detonation of several charges, a short description of the blast output from a single charge is appropriate.

When an explosive source is detonated, the rapid release of energy causes a sudden increase in pressure in the immediate vicinity of the source. The region of high pressure or shock front is characterized by a near instantaneous increase from ambient conditions (i.e., pressure, particle velocity, density and temperature) to peak shock front conditions. The shock front expands radially from the center of the source at a decreasing rate. The time variations of blast parameters of pressure, density, particle velocity and temperature at any point away from the charge center have similar characteristics. Pressure is shown in The shock front arives at the point in question at some time, ta, and the pressure rises almost instantaneously to the peak value, Ps. The pressure then decays exponentially to the ambient pressure in a time, 'd. The period from the initial arrival of the shock until the pressure has decayed to the ambient conditions is known as the positive phase duration. Thereafter the pressure drops below the ambient condition for a time longer than the positive phase before returning to the initial value. This period is known as the negative phase duration. Although all of the blast parameters are somewhat similar, the actual positive and negative phase durations for pressure are not necessarily the same for the other shock front parameters.

Consider now the case of three charges detonating simultaneously. The three charges will each produce separate shock fronts which will arrive at some point in space, sequentially. As the observation point moves farther from the charges, the later arriving shock waves will begin to overtake the initial shock. This is because the initial shock front compresses and heats the undisturbed air as it passes through, and in addition, imparts a velocity to the air particles in the direction of shock propagation. Therefore, the subsequent shocks travel through a warmer, denser environment than the initial shock which is also moving in the direction of travel of the first shock. Since the shock velocity of a gas is an increasing function of temperature, the secondary shocks will travel faster than the initial shock. At some point in space, the three individual shocks will coalesce and be similar at the same distance to a shock generated from a single explosive charge with a mass equal, to the total of the three charge masses. Thus the characteristic shape of the pressure at some point in space may vary from a single shock front, such as in Figure 1, to three distinct shock front arrivals. Factors governing the type of pressure trace obtained at a given location are the size of the individual charges, the distance between charges and the location of the point in question.

Blast Parameter Scaling

Experimental studies of blast wave phenomena are often difficult and expensive, particularly when conducted on a large scale. Methods of computation of blast wave characteristics are often so involved that one cannot economically repeat these computations while varying, in a systematic manner, all of the physical parameters which may affect the blast wave. Almost from the outset of scientific and engineering studies of air blast, various investigators have attempted to generate model or scaling laws which would widen the applicability of their experiments or analyses.

The most common form of scaling, familiar to anyone who has had even a rudimentary introduction to blast studies, is Hopkinson or "cube-root" scaling. This law was first formulated by B. Hopkinson (Reference 3) and independently by C. Cranz (Reference 4), and states that self-similar blast waves are produced at identical scaled distances from two explosive charges of similar geometry and identical explosive material, but of different size, which are detonated in the same atmosphere. The implications of Hopkinson-Cranz scaling can perhaps be best described by the example illustrated in Figure 2. An observer located a distance R from the center of an explosive source of characteristic dimension d will be subjected to a blast wave with amplitude (peak overpressure) P, duration t_d, and a characteristic time his tory. The positive impulse 1 of the blast wave, defined by

$$I = \begin{cases} t_a + t_d \\ t_a \end{cases} p(t)dt$$
 (1)

where t_a is arrival time of the shock front and p(t) is the wave form of the time-varying overpressure, is often used to characterize the blast wave. The Hopkinson-Cranz scaling law then states that an observer stationed a distance λR from the center of a similar explosive source of characteristic dimension λd detonated in the same atmosphere will feel a blast wave of similar wave form, identical amplitude P, duration λt_d , and impulse λl . All characteristic times such as arrival time t_a are scaled by the same factor as the length scale factor λ . In such scaling, both pressures and velocities are unchanged at homologous times.

Hookinson-Cranz scaling has been shown by many investigators to apply over a very wide range of distances and explosive source energies. An example of early published work is that of Stoner and Bleakney (Reference 5) which showed that such scaling would apply for a limited range of distances and source energies. The list of other investigations corroborating this law is too lengthy to include here, but a report by Kingery, et al., (Reference 6) showing very good agreement between blast data obtained during a field test with a 100-ton TNT detonation and predicted values scaled from experiments with 1- to 8-1b charges, will serve to indicate the usefulness of this ubiquitous law. It has, in fact, become so universally used that blast data are almost always presented in terms of the Hopkinson-scaled parameters:

$$Z = R/W^{1/3}$$
 (scaled distance)
 $T = T/W^{1/3}$ (scaled time) (2)
 $\zeta = 1/W^{1/3}$ (scaled impulse)

This law implies that all quantities with dimension of pressure and velocity are unchanged in the scaling. Thus, side-on pressure, dynamic pressure, and reflected pressure all remain identical at homologous times, and both shock velocity and time histories of particle velocity are unchanged.

Model Analysis

In a program such as this one, it is often beneficial to conduct a model analysis prior to the beginning of testing. The purpose of the model analysis is to design a series of scaled experiments which will simulate in a realistic fashion the pressure-time histories of large-scale or projetype detonations of multiple charges. The problem addressed by the model analysis developed below is that of three charges detonating simultaneously. The charges are suspended above an infinitely long, infinitely wide and infinitely stiff reflecting surface. The object of the model analysis is to develop the scaling relationships for the pressure and impulse which are applied at various points along this surface.

The first step in developing a model analysis is to list all the parameters which are required to characterize the phenomena. Table 1 is a list of the 24 parameters which are required to characterize the explosive charge, the atmospheric conditions, the shock front, charge locations and the reflecting plane. To characterize the explosive charge, the energy release of the explosive, E, charge radius r, density ρ_e , detonation velocity a_e , and the explosive products specific heat ratio γ_e are required. The effective limit for explosive detonation g is listed because, as is well known, there exists a minimum charge linear dimension below which it is impossible to initiate or propagate a detonation. This parameter will define a lower limit for the scale at which the tests will be conducted.

The medium in which the detonation occurs is characterized in the analysis by the ambient air pressure P_a , sonic velocity in air a_a , ambient air density ρ_a , ambient air temperature θ_a , the specific heat ratio of air, γ_a and the specific entropy, S. The shock itself is characterized by the velocity \textbf{U}_i , gas density ρ_s , particle velocity \textbf{u}_s and a shock front temperature θ_s .

The remaining parameters are used to characterize the geometry of encounter and the responses to be measured. In this program it is desired to measure the pressure P and impulse I as a function of time t, as well as the arrival time of the shock wave t_a and the shock wave duration t_d . The position of the point where responses can be determined by three coordinates: the standoff distance R, the shock front encounter angle Φ , and the spacing between charges, s_1 .

The second step in developing a model law is the derivation of scaled quantities, called pi-terms, from the list of important parameters. The procedure of deriving the pi-terms is described in Chapters 2 and 3 of Reference 7. For brevity, only the resulting pi-terms are presented here. Twenty pi-terms can be derived from the 24 parameters listed in Table 1. One possible set of pi-terms, or nondimensional quantities, is listed in Table 2.

The first four pi-terms are statements of geometric similarity. That is, all lengths in the prototype must be scaled by the constant λ in the model for the two systems to be equivalent. The shock wave encounter angle Φ is identical in equivalent systems. Pi-terms five to seven state that similiar explosives must be used in the model and prototype systems, and pi terms six to eleven require that similiar atmospheres exist in the model and prototype systems.

Pi-terms 13 to 19 are the response pi-terms in this analysis. These terms impose no restrictions on the model, but rather define how to scale the model measurements of pressure, impulse, arrival time and duration in order to make prototype scale predictions of the same parameters.

All twenty pi-terms listed in Table 2 can be satisfied providing replica modeling is used. In a replica model, the same materials are used in the model and prototype systems, and all geometric quantities are scaled by the scale factor λ . By examination of the remaining pi-terms, the scale factors for quantities other than length can be established. The use of the same explosives and atmosphere in the two systems implies that all densities, temperatures and specific heats will be identical in the model and prototype systems. Since the same atmosphere is used, pi-terms 7 to 9 further imply that velocities and pi-term 16 implies that pressure will be invariant between systems. That the scale factor for energy is λ^3 can be established by observing π_{16} and noting that the scale factors for pressure and length are 1.0 and λ respectively. Similarly, π_{19} shows the scale factor for time is λ .

Table 3 summarizes the replica scaling law for miltiple detonations. The replica model law is essentially an extention of the Hopkinson-Cranz scaling of blast parameters. Several pi-terms have been added to account for the extra parameters needed to characterize the test geometry and to account for the fact that the initial blast front compresses, heats the initially undistrubed air and imparts a net velocity in the direction of shock front propagation.

The model analysis developed above was used to design the model experiment so that the prototype situation, three charges detonating simultaneously near a reflecting plane, could be modeled accurately, and so that the parameters required to created a blast-resistant structure would be available. The designer primarily needs to know the pressure and impulse acting on a structure and he will sometimes use duration measurements when they are available. Arrival time measurements are useful when multiple shock fronts are present.

If one were to write an equation for the pressure, impulse, time of arrival or duration at some point on the target, he would be defining a 12 parameter space. That is, each of the responses is a function of the first 12 pi-terms in Table 2. However, many of the parameters in each of the pi-terms are essentially constant and may be eliminated from the analysis without significant loss of accuracy. For example γ_e , ρ_e , ae, P_a , a, ρ_a , γ_a and θ_a are all invariant. If the size of the charge is above the minimum size required to sustain detonation, the effective limit for explosive detonation g may be ignored. Under these circumstances, the following functional relationships for pressure, impulse, arrival time and duration can be written:

$$P = f_1\left(\frac{r}{R}, \frac{s_1}{R}, \phi, \frac{R}{E^{1/3}}, \frac{t}{R}\right)$$
 (3)

$$\frac{I}{E^{1/3}} = f_2\left(\frac{r}{R}, \frac{s_1}{R}, \phi, -\frac{R}{E^{1/3}}, \frac{t}{R}\right)$$
 (4)

$$\frac{t_a}{E^{1/3}} = f_3\left(\frac{r}{R}, \frac{s_1}{R}, \Phi, \frac{R}{E^{1/3}}\right)$$
 (5)

$$\frac{t_{d}}{E^{1/3}} = f_{4}\left(\frac{r}{R}, \frac{s_{1}}{R}, \phi, \frac{R}{E^{1/3}}\right)$$
 (6)

In this program only one explosive type will be used; therefore, the parameter E can be replaced by the charge weight W, resulting in a more familiar form for Equations 3 to 6. In addition, if we recognize that only the peak value of pressure and the impulse will be used by designers, the following relations are obtained:

$$P = f_1\left(\frac{r}{R}, \frac{s_1}{R}, \phi, \frac{R}{w^{1/3}}\right)$$
 (7)

$$\frac{1}{w^{1/3}} = f_2\left(\frac{r}{R}, \frac{s_1}{R}, \phi, \frac{R}{w^{1/3}}\right)$$
 (8)

$$\frac{t_a}{w^{1/3}} = f_3\left(\frac{r}{R}, \frac{s_1}{R}, \Phi, \frac{R}{w^{1/3}}\right)$$
 (9)

$$\frac{t_d}{u^{1/3}} = f_4\left(\frac{r}{R}, \frac{s_1}{R}, \phi, \frac{R}{u^{1/3}}\right)$$
 (10)

The data accumulated during this program can be used to predict full scale measurements of P, I, t_a and t_d provided the prototype experiments use the same explosive and the measurements are made over the same range of values of the six parameters in the above functions. The equation relating the four responses to the independent variables is not derived as part of this program; instead the data are presented in a graphical form. Only the peak values of the pressure and the impulse are presented and all four responses are plotted as a function of ϕ and $R/W^{1/3}$. Separate plots for the different charge geometries are presented.

EXPERIMENTAL PROGRAM

General

The objective of this test program was to investigate the blast effects on a barricade due to the simultaneous detonation of three charges at small scaled distances. To accomplish this objective, a technique for measuring the blast pressures and impulses at scaled distances of 0.32 to 1.2 m/kg $^{1/3}$ (0.80 - 3.0 ft/lb $^{1/3}$) was devised. The program consisted of exploding either one or three spherical Composition B charges at various distances above the ground surface. The Composition B charges were cast by The Explosive Processing group of the Naval Surface Weapons Center, White Oak Laboratory, Maryland, and had relatively uniform mass and diameter. Pressure-time histories were recorded with piezoelectric transducers mounted in metal canisters buried in the ground. Impulse measurements were obtained by integrating the pressure-time histories.

The program consisted of four series of tests as summarized in Table 4. In Test Series 1, a single charge weighing either 0.65 kg (1.43 lb) or 2.29 kg (5.05 lb) was detonated from 0.29 to 1.56 m (0.95 - 5.13 ft) above the reflecting plane. This series of tests was conducted to validate the experimental technique and transducer calibration by generating data which could be compared directly with data in the literature. In addition, this series of tests served as a baseline from which the effects of three charges detonating simultaneously could be evaluated. Test Series 1A was conducted to examine the validity of the model law by detonating a different scaled size charge at an equivalent scaled distance. A total of 15 Series 1 tests was conducted at four different scaled distances: 0.335, 0.5, 0.672, 1.2 m/kg $^{1/3}$ (0.84, 1.25, 1.70, 3.0 ft/lb $^{1/3}$). A schematic diagram of the charge placement and gage positioning is given in Figure 3a.

Test Series 2 was conducted to determine how the blast output of three charges which are grouped together differs from the blast output of a single charge. The test configuration for this series is shown schematically in Figure 3b. Notice that the standoff distance R is measured in this case as the distance from the ground surface up to the center of mass of the three charges. A total of nine tests at the three scaled distances, Z = 0.478, 0.716 and 0.960 m/kg¹/3 (1.2, 1.81, 2.42 ft/1b¹/3), was conducted in Test Series 2. For the grouped array tests, the total weight of the three charges was used in computing the scaled distance Z. This convention facilitates comparison with the single charge test results.

Test Series 3 was conducted to investigate the variations of blast output of three charges which are distributed in a horizontal array for various charge spacings and standoff distances. The test configuration for this test series is shown schematically in Figure 3c. A total of 16 tests was conducted in this test series. Three scaled distances were investigated, Z=0.719, 0.960 and 1.19 m/kg $^{1/3}$ (1.81, 2.42, 3.01 ft/1b $^{1/3}$), as well as three charge spacings, s=0.366, 0.71 and 1.07 m (1.2, 2.33 and 3.5 ft). Of particular interest in this test series was the possibility of regions of enhanced pressure or impulse at gage locations between charges over what would be expected if only one charge was present.

The final test series was designed to investigate the blast output of three charges which are placed in a vertical array. This situation is shown schematically in Figure 3d. A total of four tests was conducted at a scaled distance, $Z=0.51~\text{m/kg}^{1/3}$, $(1.29~\text{ft/lb}^{1/3})$, and a charge spacing of 0.145 m (0.475 ft). As was the case for the grouped charge arrays, the standoff distance, R, is measured from the ground surface to the center of mass of the three charges, and W is the total charge weight. This convention is used to facilitate comparison with the single charge test results.

Transducer Placement

In order to perform the measurements, a reflective surface, capable of withstanding the loads due to the exploding charges and of holding the transducers in place, had to be designed. After some consideration, it was decided to use the ground as the reflecting plane rather than a more conventional test stand, because in some tests the three charges would have a separation distance of as much as 2.08 m (6.8 ft). In order to satisfy the assumption in the model analysis that the reflecting plane was effectively infinite in extent in all horizontal directions and infinitely stiff, a conventional steel test stand would have to be wider, longer and thicker than was practical, therefore, the ground, which has infinite dimensions and stiffness, was chosen as the most advantageous reflecting plane.

The gages were installed in separate fixtures, as shown in Figure 4. Each canister had provisions for removing the surface plate so that the transducer and cable could be serviced without taking the canister out of the ground. The bottom cavity of the canister in Figure 4 was designed to hold several coils of microdot cable, to allow enough slack to remove the cover plate and transducer. The cable exited the canister through a NPT coupler and up to the ground surface. The portion of the cable outside the canister was encased in 1.59 cm (0.625 in) garden hose. Water tightness of the entire assembly was assured by using gaskets between the surface and base plates, and by sealing both ends of the garden hose with silicon rubber.

Three different transducer types were used in this program, and all three types could be used with the canisters. The PCB 102A03 transducer threaded directly onto the surface plate as shown in Figure 4. The remaining two transducer types threaded into cylindrical plugs 3.19 cm (1.25 in) in diameter and 3.10 cm (1.22 in) tall. Steel plugs were used with the PCB 109A02 gages while silicon rubber plugs were used with Susquehanna Instruments ST-2. The plugs protruded slightly above the canister body so that no movement of the plug was possible once the surface plate was installed. The transducer protruded 0.635 cm (0.25 in) above the canister body so that the sensitive diaphragm was flush with the surface plate. Gaps between the transducer and surface plate were filled with modeling clay to provide a uniformly flat top surface.

The canisters were buried in the ground so that the surface plate and the transducer diaphragm were flush with the ground surface. The transducer cable enclosed by the garden hose exited the ground a minimum of 1.22 m (4.0 ft) from the gage line. The nine canisters were buried at 0.361 m

(1.18 ft) intervals. Once the transducers were placed, they remained in the ground in their original positions until the test program was completed.

Test Procedure

All 44 tests were performed at an outdoor explosives site on the SwRI grounds. A typical test was conducted by first installing the pressure transducers in the nine canisters. The type of transducer installed at any measurement location was determined by the pressure expected to be generated by the test. While the instrumentation was being readied, the ground surface surrounding the canisters was leveled. On many occasions it was easier to remove the top 0.8 to 1.6 cm (0.31 - 0.62 in) of soil and replace it with new soil, as previous tests had compacted the soil to the point where it was unworkable. After the ground surface and instrumentation was prepared, the charge was suspended from a bar 2.44 m (8 ft) high at the correct standoff distance above the ground. The charges were held in place above the gage line by light string running to two points on the ground as shown in Figure 5. After all charges had been secured, a final electrical continuity check of all firing and instrumentation lines was made; the detonators were placed in the center of the spherical charges and positioned so that no fragments would be likely to strike the transducer. The detonators used in this program were Reynolds Industries RP-81 electronic bridgewire detonators. These EBW's are used extensively where simultaneity of detonation of multiple charges is desired. When connected in series, up to 8 charges can be detonated with a simultaneity not worse than 0.125 µs. After the detonators were placed and the area cleared, the exploding bridgewire firing system was triggered. The data were recorded on magnetic tape and five channels were backed up by Biomation recorder. Oscillograph records were made from the data on magnetic tape and polaroid prints made of the Biomation recordings. Typical damage to the ground surface produced by a test is shown in Figure 6.

Instrumentation System

Several different transducers were used in this project to obtain the pressure-time data. Each transducer was selected depending on the peak pressure expected at a given measurement location. The majority of the data were recorded using piezoelectric transducers, although a few measurements were made with a piezoresistive type.

The piezoelectric transducers utilize a ceramic or crystal to generate an electrical charge which is proportional to the stress imparted by the blast wave. Two models, 102A03 and 109A02, made by PCB Piezotronics and one model, ST-2, made by Susquehanna Instruments were used in this project. The PCB transducers use a quartz sensing element with a resonant frequency of 500 kHz. The model 102A03 has a pressure range of 6.9 to 138,000 kPa (1-20,000 psi), while the model 109A02 has a range of 13.8 to 827,000 kPa (2-120,000 psi). These two models are made to withstand up to 20,000 g's of shock acceleration. They contain a built-in amplifier which provides a low impedence, voltage-mode output for improved signal-to-noise ratio, long-line driving capability and good low frequency response as compared to the high impedence, charge-mode output of other piezoelectric transducers.

The Susquehanna ST-2 transducer uses a lead-metaniobate sensing element having a natural frequency of 250 kHz and a pressure range of 0.69 to 3,450 kPa (0.1 to 500 psi). The one piezoresistive transducer used was a Kulite Model HFG-375-1,000 having a natural frequency of 500 kHz and a pressure range of 0-6,000 kPa (0-1,000 psi). This unit was balanced, calibrated and powered with a B&F Model 1-700 signal conditioner. The output was amplified with a B&F Model 702A-100 differential amplifier having a frequency response of 0-100 kHz before being recorded on magnetic tape.

The piezoelectric transducers were connected as shown in Figure 7. Their outputs were also recorded on an Ampex FR-1900 Wideband II magnetic tape recorder which has frequency response of 0-500 kHz at a record speed of 3.05 m/s (120 ips). The data were played back with a reduction speed ratio of 64 into a Bell & Howell Model 1-124 oscillograph recorder with a 5 kHz CEC response galvanometer. The resultant frequency response of the playback system was then 0-320 kHz. For quick-look analysis, the output of some of the transducers was redundantly recorded on Biomation Models 802 and 1015 transient digital recorders with a frequency response of at least 0-50 kHz.

The pressure transducers were dynamically calibrated using a hydraulic calibrator consisting of a triangular chamber filled with oil. Two symmetric ports are provided for flush mounting a reference and a test transducer. The pressure pulse is generated by dropping a weight down a guide tube onto a piston which extends through the top of the chamber. This device produces a half-sine, positive pressure pulse with peak amplitudes from 0.7 MPa (100 psi) to more than 100 MPa (14,500 psi) and rise times of 1 to 2 milliseconds. Different weights and drop heights are used to vary the peak amplitudes. Figure 8 shows samples of typical calibration pressure pulses. The reference piczoresistive transducer used was first calibrated using a dead-weight hydraulic tester to check its sensitivity. It in turn, was used to determine the pressure input to the test transducer.

Data Reduction

The oscillograph traces and polaroid photographs obtained from each test were used to obtain peak pressures, positive impulses, arrival times and positive phase durations. The data were reduced by manually digitizing the records using a Hewlett-Packard Model 9830 microprocessor and a Herlett-Packard Model 9864A digitizing plotter. The BASIC program which has used to digitize the pressure-time traces also performed the following services:

- 1. integrate the pressure-time trace
- retain peak positive impulse
- retain arrival time of each blast front
- retain peak pressure associated with each blast front arrival
- 5. retain total positive duration

The pressure impulse and time traces were plotted for each test in the format shown in Figure 9. In addition, the pressure-time trace was stored on magnetic tape along with Items 2-5 listed previously. After all the data had been reduced for a given test, a separate program was used to print a summary of Items 2-5 in a convenient form for checking errors and plotting the data. The data are printed by this program in both scaled and raw form.

EXPERIMENTAL RESULTS

General

The results of the experimental program are presented in this section in graphic—form. The scaling law derived in the model analysis and presented in equations 7-10 states that pressure, impulse, positive duration and time of arrival are a function of the scaled distance Z, the scaled charge separation s_1/r and the shock front encounter angle \diamondsuit *. In the general solution, a five parameter space must be considered to properly scale the data. The results presented in this section, however, define a four parameter space. This is because the scaled charge size, r/R, was held relatively constant during the test program $(0.0425 \le r/R \le 0.154)$. This fact does not negate the model law, but only places a restriction that the use of this data be limited to situations where r/R is in the range of 0.0425 to 0.154. Care should be exercised whenever the data presented in this report is used for predictions outside this range in r/R.

In this section, graphs of pressure, scaled specific impulse, scaled positive duration and scaled time of arrival are presented as a function of the scaled position. At each value of x/R, the average response parameters, along with the maximum and minimum recorded values, have been plotted while taking advantage of the symmetry about P5 in the transducer array. Measurements at Pl and P9, for example, are plotted together. Where appropriate, two curves are presented on each graph. The first is a solid line drawn through the average points as near as possible while maintaining a smooth transition from point to point and the correct slope (zero) at x/R = 0. The second line is transferred from the appropriate single charge figure and is presented such that the relative blast output of a single charge versus multiple charges can be visualized in a convenient manner. In order to easily visualize the differences between different scaled distances or charge spacings, all of the plots for a given blast parameter are presented on one page for each of the four test geometries. Each figure is labeled to indicate the test series, the scaled standoff distance and the scaled charge separation distance. All of the pressure, impulse, duration and arrival time data presented in this section appear in tabular form in Appendix A. For the convenience of the reader, the data are presented on the figures and to the Appendix in both metric and English units.

Pressure Data

The peak pressure data accumulated during this program are shown in Figures 10 to 14. Figure 10 summarizes the peak pressures resulting from the detonation of a single charge at four scaled distances from a reflecting surface. Two scaled charge sizes were investigated in the single charge tests to validate the model analysis (0.68 kg (1.5 lb) and 2.29 kg (5.05lb)). Since the charge size was scaled as dictated by π_1 of the model law, one would expect pressure to be a function of only the position at which it was

For convenience in presenting the data, the angle Φ will be represented on the figures and in the discussions which follow by its horizontal (x) and vertical (R) components.

measured. This is demonstrated by the A and B series tests $(Z=0.50 \text{ m/kg}^{1/3} (1.25 \text{ ft/lb1/3}))$ and the R and S series tests, (Z=1.19 m/kg1/3 (2.99 ft/lb1/3)) where a single line—can be drawn through all of the test data. Note that there is a consistent trend in the four pressure curves shown in Figure 10. As the measuring point moves away from directly under the charge (x/R=0), the peak pressure decays very slowly until x/R approaches 0.2. This narrow region of gradual pressure change is followed by a region in which the pressure decays substantially until x/R is about 1.5. For values of x/R greater than 1.5, the decay of pressure with increasing x/R is again quite gradual. These three regions may be conveniently thought of as (a) essentially reflected pressure, (b) transition from reflected to side—on pressure and (c) a region which approximates side—on pressure.*

The pressure generated by three 0.23 kg (0.51 lb) charges grouped together as in Figure 3b, is shown in Figure 11. Three different scaled distances were investigated for this charge configuration. The solid curve in Figure 11 represents an "eveball" fit to the data generated by the grouped array. The dashed line represents the single charge data for equal scaled distances. Note that the comparisons given in Figure 11 are between three 0..3 kg (0.51 lb) charges and a single 0.65 kg (1.43 lb) charge. This comparison is not intended to demonstrate agreement between single charges and grouped charges but rather to indicate differences in magnitude and tendency. The reader is reminded that standoff distance (2) of the group array is measured to the center of mass of the three charges. The curves shown in Figure 11 exhibit a crend consistent with the variations in pressure with x/R for the single changes; however, the pressures are reduced. This reduction may be due to a lower energy density of the three charges. As expected, the gap between the pressure curves for the single charge and the grouped array decreases as x/R becomes large, subsequently coalescing at large x/R values.

Figure 12 presents the variation in pressure for three charges in a horizontal array at three different scaled distances. The charges in these tests were separated by 0.71 m (2.33 ft). Above each graph in Figure 12, the physical charge locations, relative to the location of the pressure transducers are represented by circles. This convention is used to aid the reader to visualizing the location of the charges. The comparisons shown on Figure 12 are between three 0.23 kg (0.51 lb) charges and a single 0.65 kg (1.43 lb) charge placed at equivalent scaled standoff distances from a reflective plane. The standoff distance for the horizontal array is computed as the vertical distance to the center of mass of the three charges, divided by the total mass of the explosive detonated (i.e., 0.69 kg (1.52 lb)). Again, the solid line represents the trend of the horizontal array data, and the single charge results are represented by the dashed line. Not that for series I and J, the pressure due to the horizontal array exceeds the single charge pressure curve at scaled positions of 0.5 to over 3.5. Only directly under the center charge $(0 \le x/R \le 0.5)$ is the pressure from the horizontal array less than that given by the

As x/R becomes large, the pressure curve approaches the side-on pressure which would be generated by a charge with twice the explosive mass at the same position (7). As the slant distance from the charges to the measurement position becomes larger, the pressure in the third region better approximates the side-on values.

equivalent single charge curve. This is because contributions from the outside charges arrive too late to positively reinforce the pressure measured directly under the center charge. The converse is also true; contributions from the center charge arrive too late to contribute significantly to the pressure under the outside charges. Indeed the pressures measured directly below the charges in Figure 12 are equal within the experimental scatter. The implication of this observation is that it is unfair to compare the single charge results with the pressure from 1/3 the explosive at positions directly under the charges. However, the intention of presenting the dashed line of Figure 12 was not to demonstrate agreement between the single and multiple charge results, but rather to highlight the differences, in both magnitude and general tendency, due to distributing the charge weight in a horizontal array.

To this point, the discussion of the variation in pressure due to changing the scaled standoff distance for the horizontal array concentrated on test series I and J, but not N. This is because no single charge tests at a scaled standoff of 0.83 m/kg $^{1/3}$ (2.09 ft/1b $^{1/3}$) were conducted due to an oversight when the program was planned. To place the series N results into perspective, it was decided to present the single charge curve for Z=0.67 m/kg $^{1/3}$ (1.69 ft/1b $^{1/3}$) in Figure 12. A dotted line is used to emphasize the single charge curve presented for a smaller Z-value. Note that the equivalent curve for Z=0.83 m/kg $^{1/3}$ (2.09 ft/1b $^{1/3}$) would fall somewhat below the dotted line on the series N plot because of the larger standoff distance. Note that the trends described above for the series I and J tests also apply to the series N results.

Figure 13 shows the variation in peak pressure due to charge spacing for horizontal array tests. Three different charge spacings were investigated (5.76, 11.2 and 16.8 charge diameters), while holding the scaled stand-off distance constant at $Z=0.83 \,\mathrm{m/kg^{1/3}}$ (2.09 ft/in^{1/3}). The charge location is again represented on this figure by a circle and the single charge curve for $Z=0.67 \,\mathrm{m/kg^{1/3}}$ (1.67 ft/lb^{1/3}) is presented in absence of data at $Z=0.83 \,\mathrm{m/kg^{1/3}}$ (2.09 ft/lb^{1/3}). The correct reference line would fall slightly below the dotted line on each of the figures. Several observations can be drawn from Figure 13. First note that the effect of greater charge spacings is to move the position of maximum pressure towards large values of x/R. For small charge spacings, series P, the pressure curve for the horizontal array approximates that for a single charge. Since no measurements were made between charges, it is unclear whether a region of enhanced pressure similar to that described in the previous section and shown on figure 11, exists.

For the intermediate charge spacing, series N, a narrow region of enhanced pressure exists halfway between the charges, and a broader region exists for $x/R \ge 1.0$. These two regions of enhanced pressure are due to the superposition of the blast output of the two charges nearest the measurement position. The highest pressures occur at x/R = 0.45, or halfway between charges, because at this point the shock fronts from both charges arrive simultaneously enhancing the pressure. The single charge blast output exceeds that of the horizontal array in series N for $0 \le x/R \le 0.3$ and series Q for $0 \le x/R \le 1.1$. The reasons for this apparent discrepancy were described previously, and are due to comparing the output of a single charge with that of 1/3 the explosive at equivalent distances. Beyond x/R = 0.3 for series N and 1.1 for series Q, superposition of the blast

output of the two nearest charges results in significantly higher pressures than would be observed from a single charge. Although only a narrow region in x/R was explored in these tests, it is apparent that the point where the horizontal array pressure begins to approximate the single charge results is a function of the charge spacing. Closely spaced charges will approximate single charge pressures at smaller scaled positions than widely spaced charges.

The peak pressures resulting from three charges placed in a vertical array are shown in Figure 14. In this case the charge spacing was fairly narrow, 2.28 charge diameters. The comparison shown on Figure 14 is between three 0.23 kg (0.51 lb) charges and one 0.65 kg (1.43 lb) charge. The standoff distance for the vertical array is computed in the vertical distances to the center of mass divided by the cube root of the total mass of explosive detonated. Notice that at scaled distances approaching x/R=0 and $x/R \ge 1.75$, the peak pressure for the vertical array tests exceeds that for a single charge. Unfortunately, only one combination of charge spacing and standoff distance was investigated for vertical arrays. It is therefore not clear whether regions of enhanced pressure would exist for different combinations of Z and s. Further vertical array tests should be conducted to see if the trends shown in Figure 14 apply to other charge spacings and standoff distances.

Impulse Data

The impulse data obtained by numerically integrating the pressure-time curves is given in Figures 15 to 19. All of the impulse data is plotted in scaled format as dictated by Equation 8. As noted previously, the impulse from multiple charge tests is scaled by the total charge weight detonated. Scatter in the data, represented by the line drawn from the min mum to the maximum value recorded at a given value of x/R, is generally larger for impulse than for peak pressure. Several factors contribute to the larger scatter, including thermal drift and uncertainties in determining the positive duration. The impulse for single charges at four scaled distances from a reflecting plane is shown in Figure 15. As montioned in Section III, the scaled charge size was varied in the A-B and R-S test series. According to the model law, the impulse from different charge weights (at a constant Z) can be collapsed to a single curve by scaling the impulse by the cube root of the charge weight. This is demonstrated in the A-B and R-S graphs in Figure 15.

Consistent trends in the impulse curves in Figure 15 can be observed. At small values of x/R, generally less than 0.5, the impulse decreases slightly. This region may be thought of as a region of essentially reflected impulse and corresponds to the region of essentially reflected pressure previously discussed. For values of x/R greater than 0.5, the impulse declines more rapidly.

Figure 16 presents the impulse generated by the grouped array at three different scaled distances. The general trend exhibited by the single charge tests is followed by the grouped array tests. Note that the dispartity between the single charge and the grouped array tests is not as great as was true for pressure. This is particularly true at $\kappa/R = 0$, where the impulse measured for the grouped array essentially equaled the single charge results. As is expected the impulses for the grouped array appear to converge towards the single charge results for larger values of κ/R .

Figures 17 and 18 present the variation in impulse for horizontal arrays due to variation in charge standoff and charge spacing. Note that the position of the charges has been included in these figures as was done in the previous section. All of the trends discussed in the previous section for peak pressure are directly applicable to the impulse curves. seen in Figure 17, a region of enhanced impulse is found between the two nearest charges. This region of enhanced response is more pronounced than for pressure (Figure 12). The enhanced impulse is probably caused partially by the contribution to the impulse from the third charge and by a slight elongation of the positive duration. The effect of varying the charge spacing on impulse is shown in Figure 18. Notice that the general shape of the impulse curves are quite similar to the pressure curves shown in Figure 13, but discrepancies between the horizontal array and the single charge results are generally more pronounced. The one exception to this observation occurs when the charges were spaced the farthest apart, Series Q. Here the impulse is nearly constant at 450 Pa-s/kg $^{1/3}$ (50 psi-ms/1b $^{1/3}$) over the entire range of x/R. Another observation which can be drawn from the horizontal array tests, Figures 17 and 18, is that as x/R becomes large, the curves for the single and horizontal array impulse begin to converge. This is particularly apparent for the curves shown in Figure 17. For wide charge spacings, (Series Q), the point at which the two curves begin to overlap is beyond the range of x/R tested.

The impulse resulting from three charges placed in a vertical array are shown in Figure 19. The variations in impulse with x/R is virtually the same as for pressure (Figure 14), and therefore the comments made in the section for pressure are directly applicable to Figure 19.

Duration Data

The duration data accumulated during this program are given in Figures 20-24. All of the duration data are presented in a scaled format as required by Equation 10. For multiple charge tests, the duration is scaled by the total charge weight detonated rather than by the weight of an individual charge. Scatter in the data is greater for duration than for any other parameter measured during the program. The factors contributing to the scatter are the same which affect the reproducibility of the impulse measurements: thermal drift and uncertainty in determining the time at which the pressure drops below the time axis. Several observations can be drawn from Figures 20-24, which apply to all charge geometries. First, the general trend is for the duration to gradually increase as x/R gets larger. The duration measurements were seldom below 0.15 ms/kg $^{1/3}$ (0.115 ms/lb $^{1/3}$) or greater than 1.0 ms/ $1b^{1/3}$ (0.768 ms/ $1b^{1/3}$); a change of less than one decade. Apparent exceptions to this observation are found in the duration measurements for the horizontally spaced charges (Figure 22) where the duration declines directly under the outside charge. Note, however, that as x/R increases from zero, the duration increases until the measuring point is halfway between charges. Further increases in x/R moves the measuring point closer to the outside charge, and the duration in turn decreases until the measuring point is directly under the charge. Beyond this value of x/R, the duration increases monotomically. Except for the decrease in the duration directly under the outside charge for the horizontal array, no significant variation in the duration with charge geometry was observed.

Time of Arrival Data

The time of arrival of the initial shock front is shown in Figure 25. All of the arrival time data are presented in a scaled format as dictated by Equation 9. Scatter in the data is the smallest observed during the program. All of the plots in Figure 25 present the initial shock front arrival at each gage. The distance which is used to calculate 2 for each point is the distance from the gage to the nearest charge. The charge weight used to scale the time of arrival and in computing the scaled distance is the total charge weight detonated for single charge, grouped and vertical array tests, but the weight of an individual charge for the horizontal array tests. The scaling relationships for arrival time collapse the data to where all four charge geometries could be plotted on one figure without increasing the scatter appreciably.

Comparison of Single Charge Results

Pressure and impulse are most often presented as plots of either normally reflected or side-on parameters as a function of the scaled distance ?. However, for many applications it is desirable to know the pressure acting on a reflecting surface at positions where neither side-on nor normally reflective measurements are appropriate. For this reason, Figures 26 and 27 represent a composite of data from this report and from references 7 and 9. In these figures the peak pressure and the scaled specific impulse are plotted as a function of the scaled position x/R. Each curve in these figures is for a different value of the scaled standoff distance Z, and this value is indicated on the legend in the upper left hand corner of the figures. Note that the charge weight used in computing Z and in scaling the impulse is the equivalent weight of TNT and not the weight of the explosive itself. This was done because different explosives were used to generate the original data. For example, the data from this report are based on measurements with Pentolite. Data from references 8 and 9 are based on limited measurements with Pentolite and primarily Composition C-4 measurements.

CONCLUSIONS AND RECOMMENDATIONS

A total of 44 tests was conducted at scaled distances ranging from 0.335 m/kg $^{1/3}$ (0.84 ft/lb $^{1/3}$) to 1.18 m/kg $^{1/3}$ (3.0 ft/lb $^{1/3}$). Four different charge geometries were studied: single charges and grouped, horizontal and vertical arrays. Based on the results of these tests the following observations can be made:

- (1) The validity of the model law has been verified for single charges by numerous researchers (2, 3, 4), which is consistent with the single charge data contained in this report. No attempt to verify the model law for multiple detonations was made during this project.
- (2) The pressure and impulse for grouped arrays at small scaled distances are lower than for single charges. The disparity between grouped array and single charge pressure is more pronounced than for impulse.
- (3) For horizontal arrays, regions exist where the pressure and impulse exceed what would be expected from a single charge. The location of maximum response is dependent on the charge spacing and the standoff distance, but generally is found halfway between charges. Other regions of enhanced pressure and impulse exist just beyond the outside charge. For very wide charge spacings, the pressure and impulse ar nearly constant over the entire range in x/R. For very narrow charge spacings, the regions of enhanced pressure are less pronounced than for intermediate charge spacings.
- (4) Only one combination of charge spacings and standoff distances was investigated for vertical arrays. The results indicated that two regions of enhanced pressure and impulse exist: one directly under the vertical array and another for x/R > 1.5.
- (5) The tests conducted verified the expectation that at large scaled distances, the blast parameters measured for multiple charges could approach those of a single charge. The distance at which the curves begin to coalesce is apparently the greatest for widely spaced horizontal arrays and the smallest for grouped arrays.
- (6) No significant variations in the positive duration were observed for the different test geometries.

Based on the above observations, the following recommendations are made:

(1) Although the scaling law has not been verified for multiple detonations, the measurements in this report can be used to obtain a more rational design for munition processing plants. Caution should be exercised however, when extrapolation of these results is required beyond the scaled distances, positions, or charge sizes tested.

- (2) Multiple detonation tests with several different charge size and standoff distance combinations should be planned to verify the complete model analysis.
- (3) Only one combination of scaled distance and charge spacing was investigated for vertical arrays. These tests should be repeated to determine whether the trends described in (4) of the conclusions will exist for other values of Z and s/r.
- (4) The gage placement for the horizontal array tests resulted in poor resolution of the variation in response as a function of x/R. particularly in the region between charges. Should tests of this nature be repeated in the future, more measurement positions should be provided in this critical region.
- (5) Computer programs which could predict the pressure and impulse acting on a barrier due to multiple charge detonations do not exist at the present time. A three dimensional program would be required, and even if available would be very expensive to run. A cheaper and probably as accurate prediction technique can be devised, based on empirical observation and Equations 8-10. However, the data presented in this report are probably insufficient to accomplish this goal. Therefore, further multiple detonation tests should be conducted and an attempt should be made to generate empirical prediction techniques.

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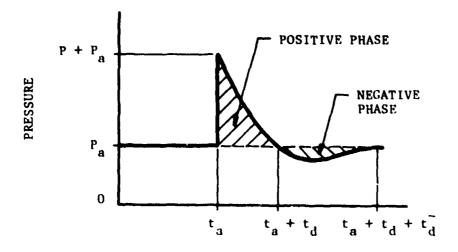


FIGURE 1. IDEAL PRESSURE-TIME HISTORY

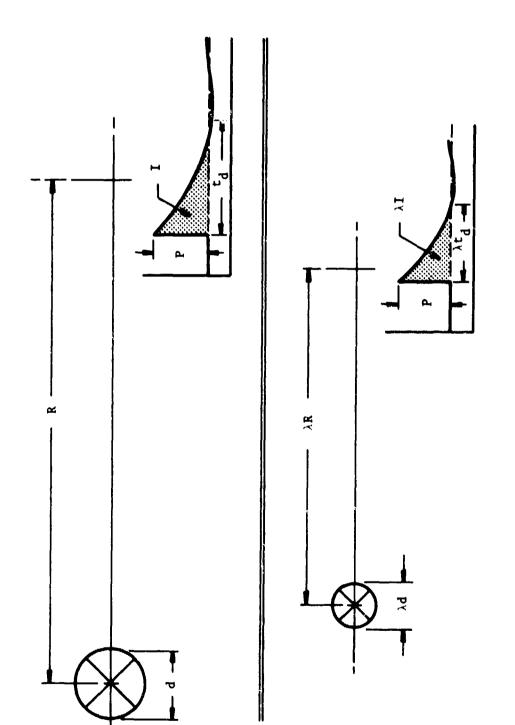


FIGURE 2. HOPKINSON-CRANZ BLAST WAVE SCALING

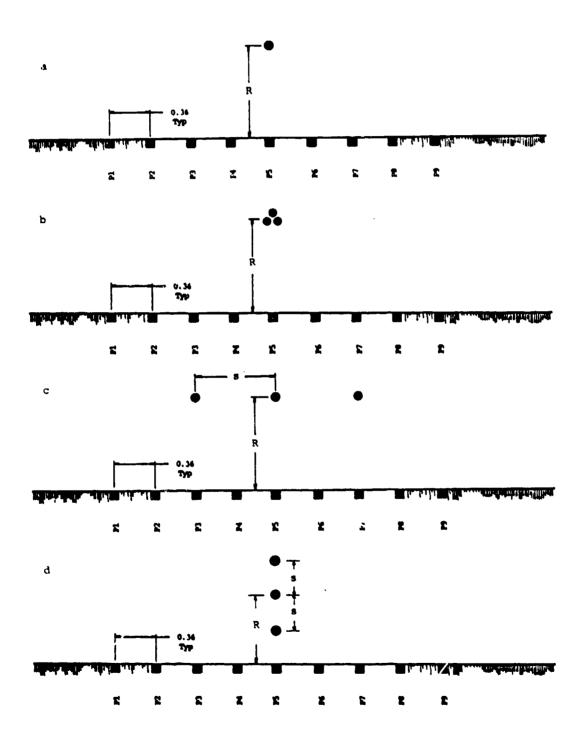


Figure 3. Transducer Arrangement and Charge Placement for the (a) Single Charge, (b) Grouped Array, (c) Horizontal Array and (d) Vertical Array tests.

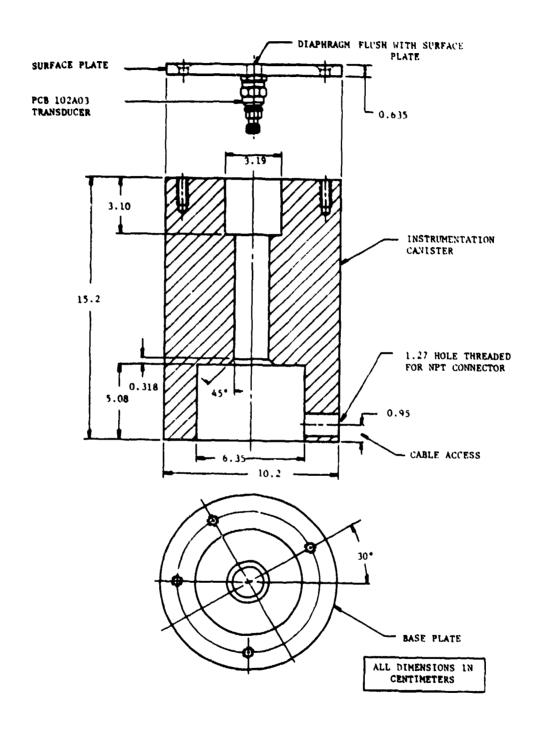


FIGURE 4. EXPLODED DIAGRAM OF THE PRESSURE MEASUREMENT ASSEMBLY

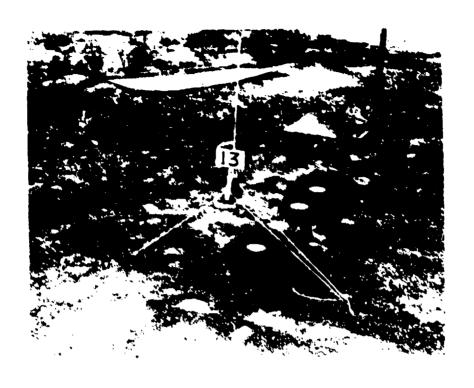
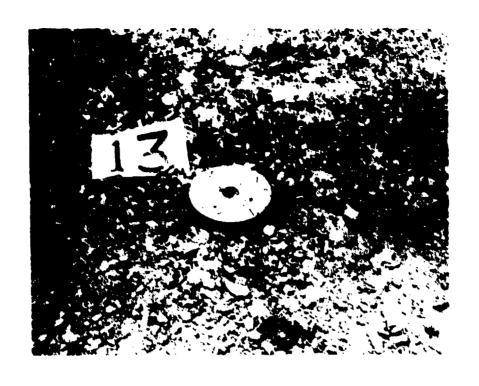




FIGURE 5. TYPICAL TEST ARRANGEMENT FOR THE GROUPED ARRAY AND THE HORIZONTAL ARRAY TESTS



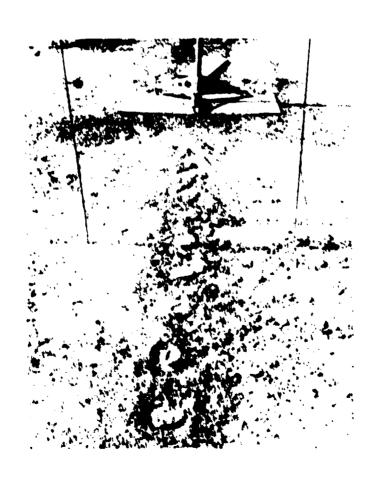


FIGURE 6. DAMAGE TO GROUND SURFACE FROM A TYPICAL GROUPED ARRAY TEST

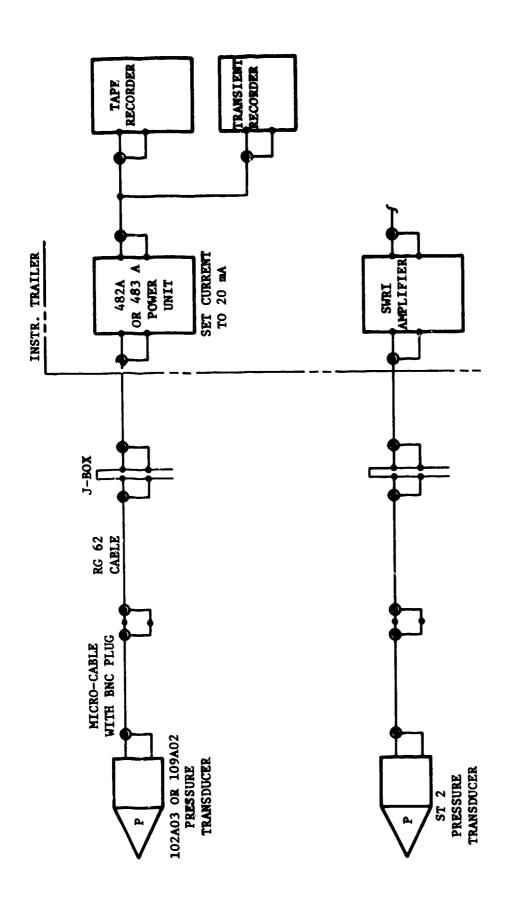
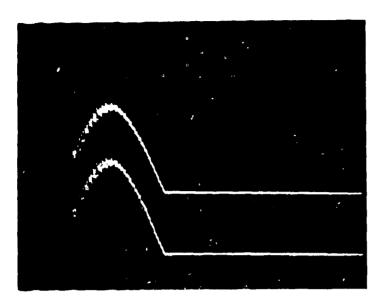


FIGURE 7. DIAGRAM OF PIEZOLLECTRIC TRANSDUCER MEASUREMENT SYSTEM



Upper Trace: Ref. Transducer

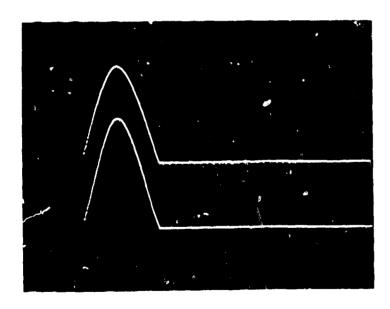
Lower Trace: Test Trans-

ducer

Peak Pressure: 38.3 MPa

(5560 psi)

Sweep: 1.0 ms/division



Upper Trace: Ref. Trans-

ducer

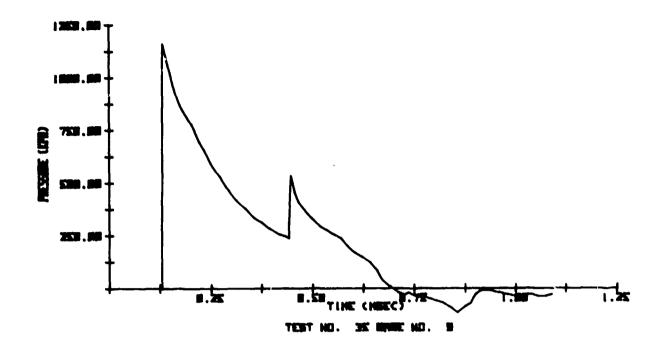
Lower Trace: Test Trans-

ducer

Peak Pressure: 46.0 MPa

(6670 psi) Sweep: 1.0 ms/division

FIGURE 8. CALIBRATION TRACES FOR PRESSURE TRANSDUCERS



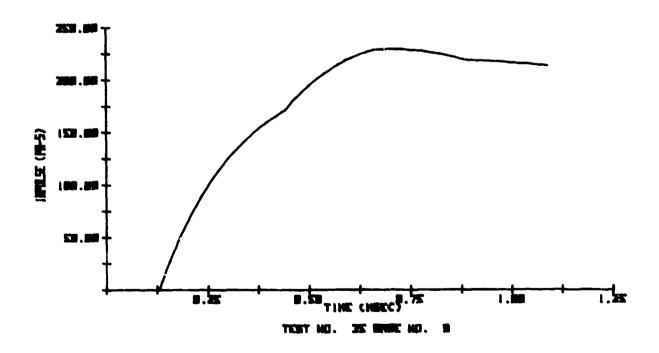


FIGURE 9. SAMPLE OF REDUCED DATA FOR GAGE 9, TEST 35 (HORIZONTAL ARRAY)

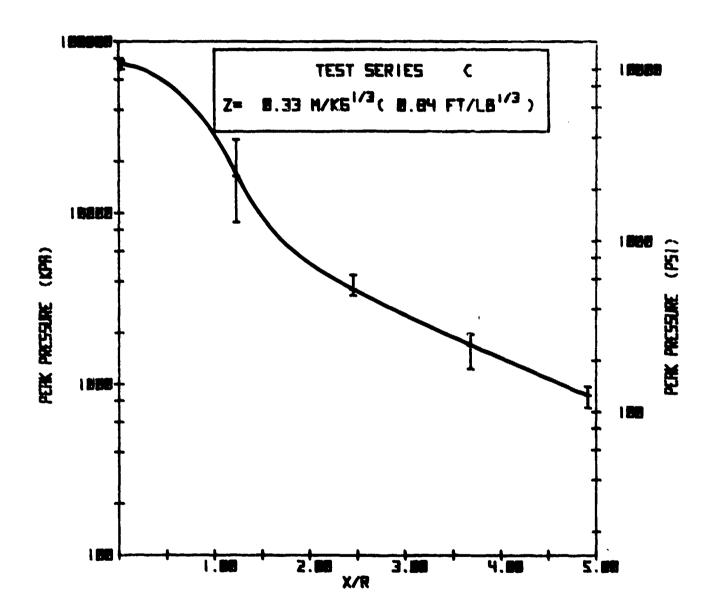


FIGURE 10. PEAK PRESSURE FOR SINGLE CHARGE TESTS

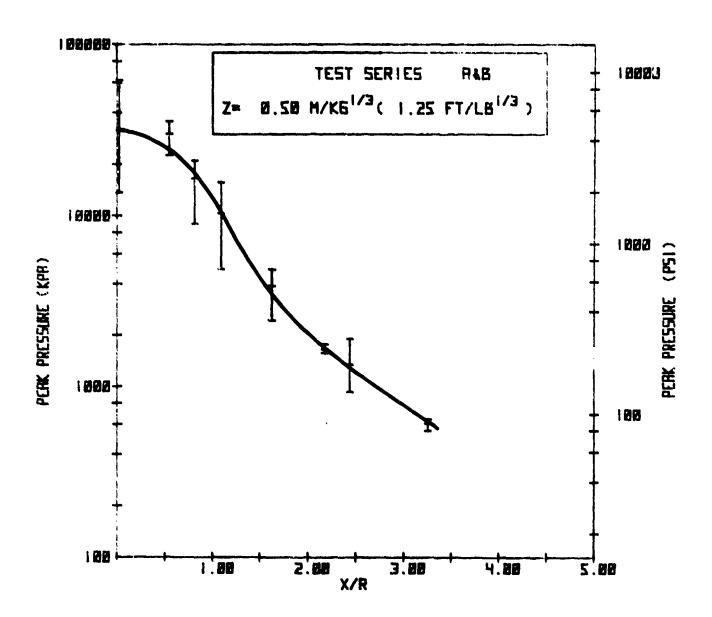


FIGURE 10. PEAK PRESSURE FOR SINGLE CHARGE TESTS (CONT'D)

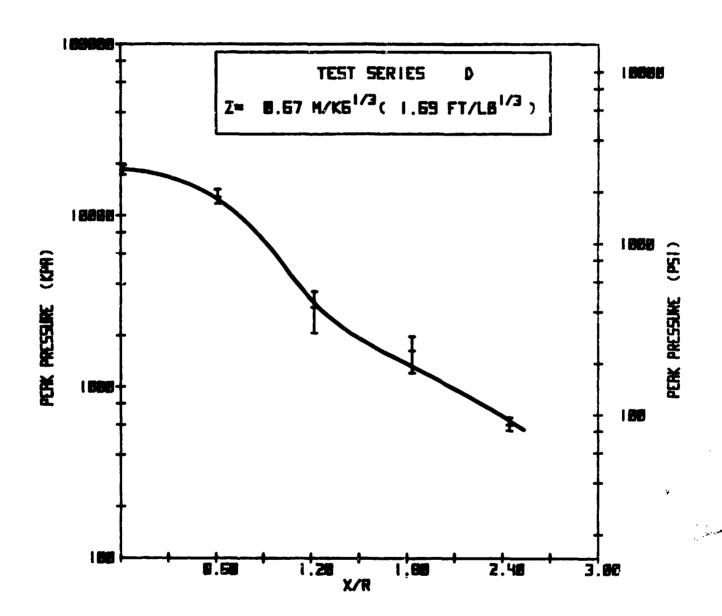


FIGURE 10. PEAK PRESSURE FOR SINGLE CHARGE TESTS (CONT'D)

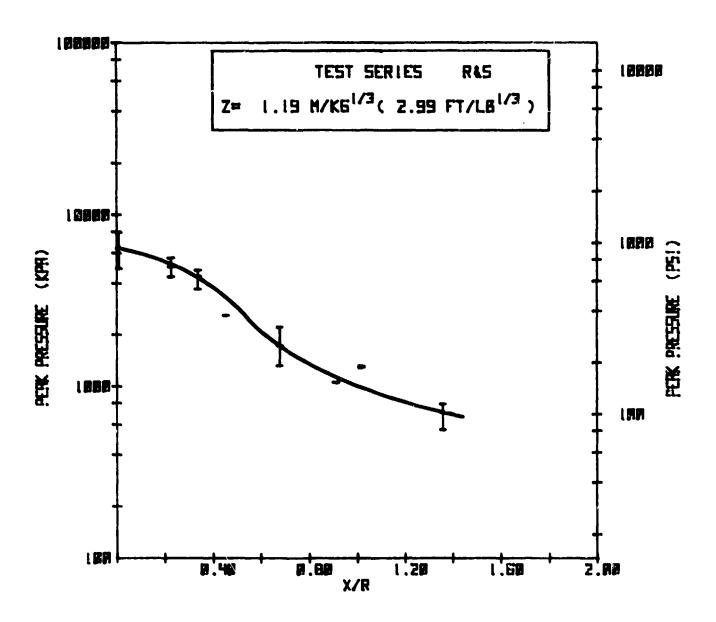


FIGURE 10. PEAK PRESSURE FOR SINGLE CHARGE TESTS (CONT'D)

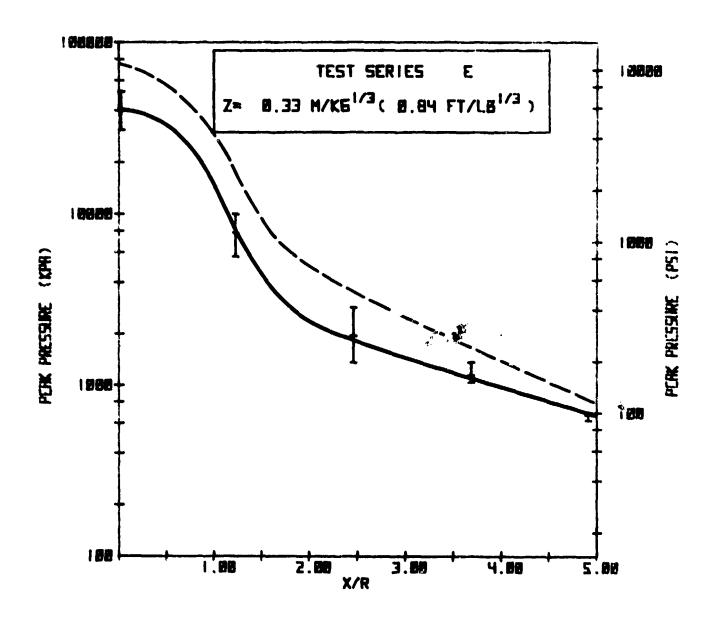


FIGURE 11. PEAK PRESSURE FOR GROUPED ARRAY TESTS

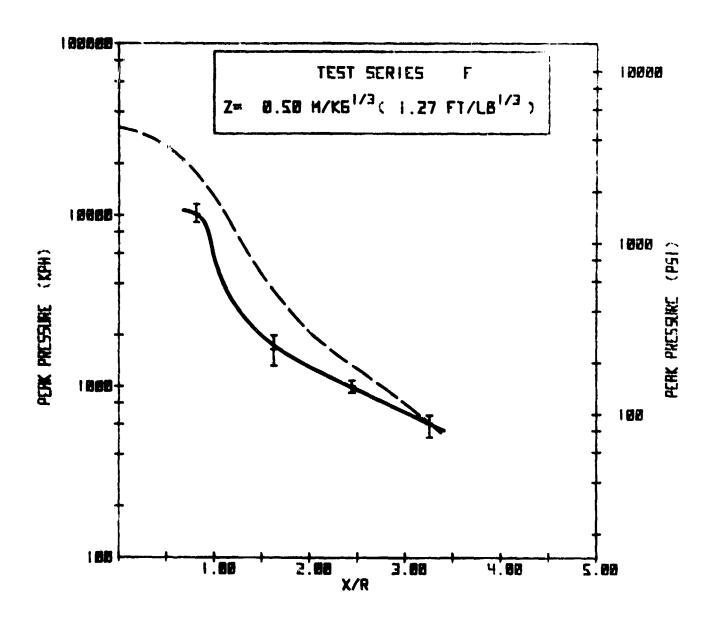


FIGURE 11. PEAK PRESSURE FOR GROUPED ARRAY TESTS (CONT'D)

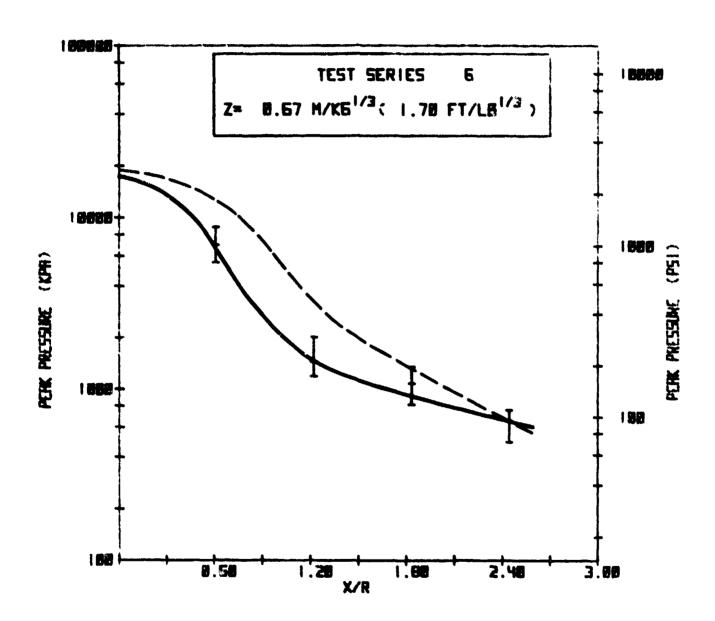


FIGURE 11. PEAK PRESSURE FOR GROUPED ARRAY TESTS (CONT'D)

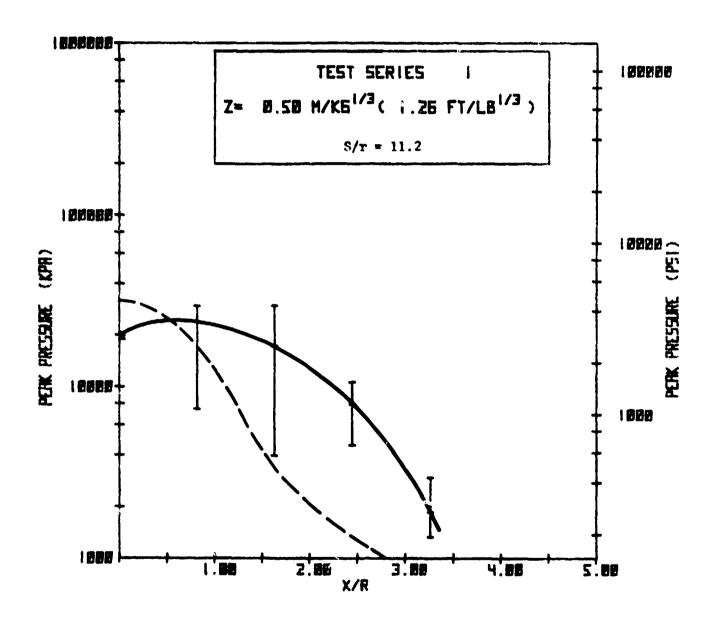


FIGURE 12. PEAK PRESSURE VARIATIONS DUE TO CHARGE STANDOFF FOR HORIZONTAL ARRAY TESTS

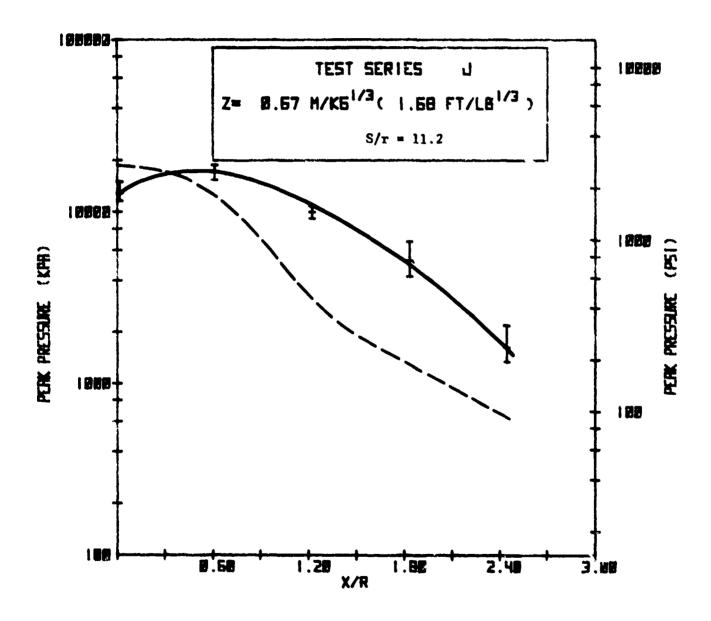


FIGURE 12. PEAK PRESSURE VARIATIONS DUE TO CHARGE STANDOFF FOR HORIZONTAL ARRAY TESTS (CONT'D)

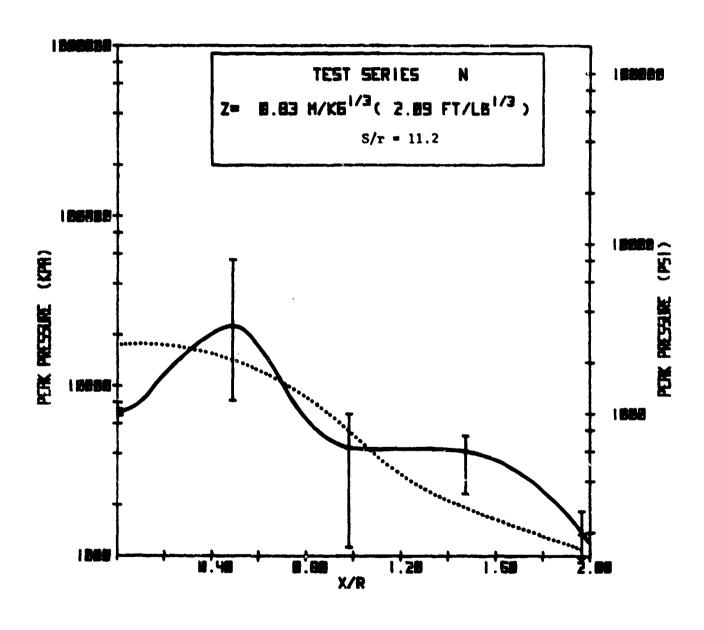


FIGURE 12. PEAK PRESSURE VARIATIONS DUE TO CHARGE STANDOFF FOR HORIZONTAL ARRAY TESTS (CONT'D)

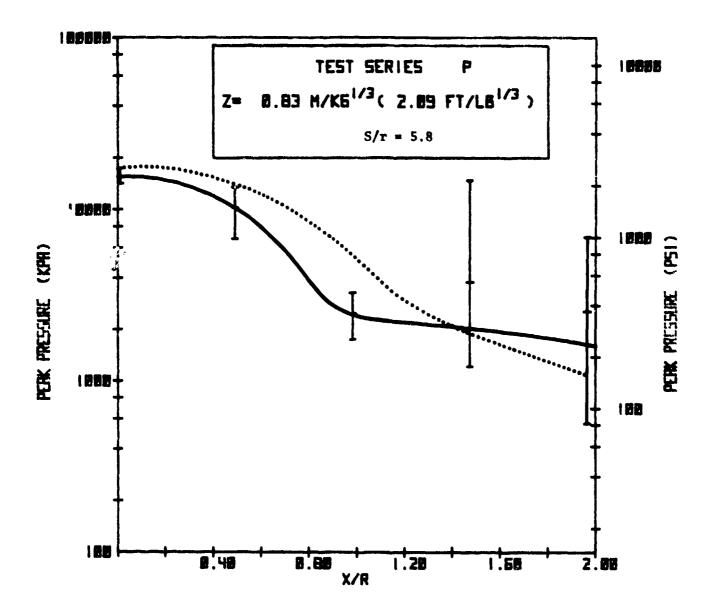


FIGURE 13. PEAK PRESSURE VARIATIONS DUE TO CHARGE SPACING FOR HORIZONTAL ARRAY TESTS

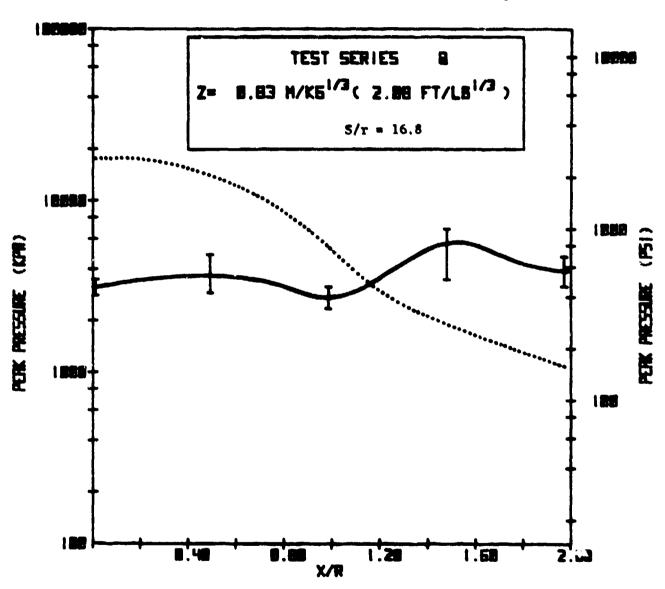


FIGURE 13. PEAK PRESSURE VARIATIONS DUE TO CHARGE SPACING FOR HORIZONTAL ARRAY TESTS (CONF'D)

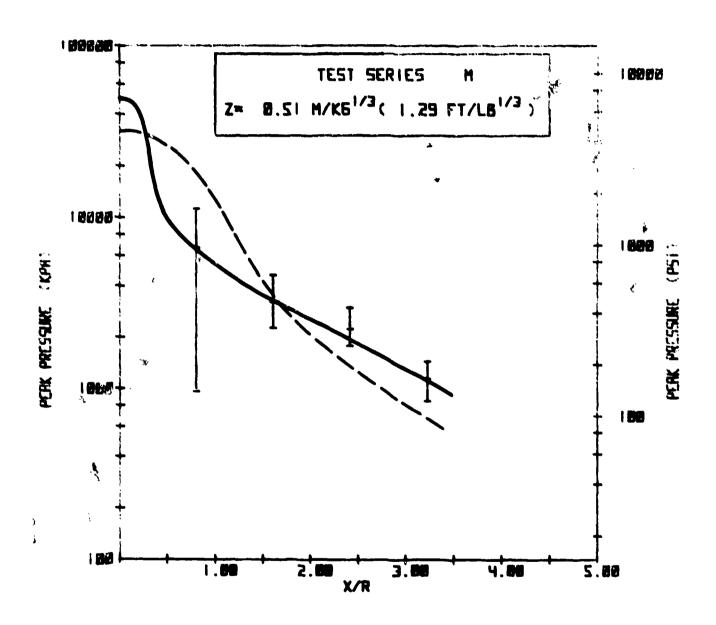


FIGURE 14. PEAK PRESSURE FOR VERTICAL ARRAY TESTS

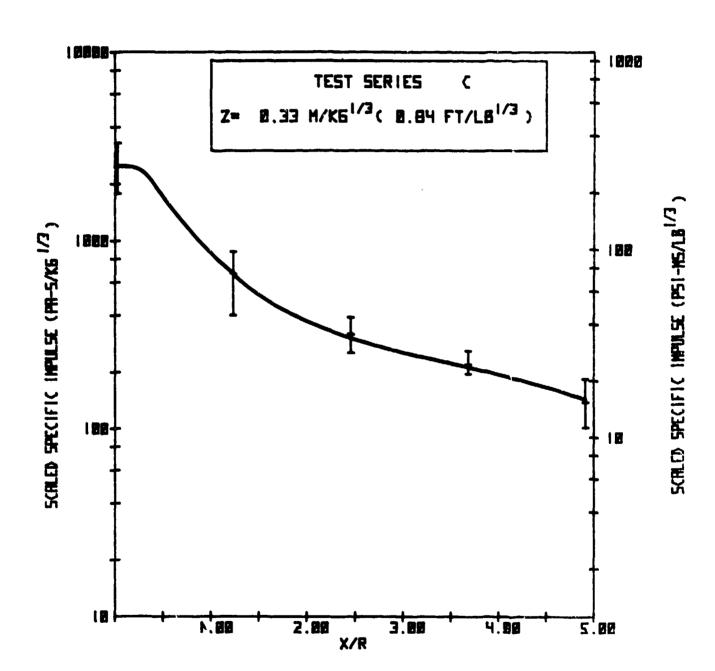


FIGURE 15. SPECIFI. AMPULSE FOR SINGLE CHARGE TESTS

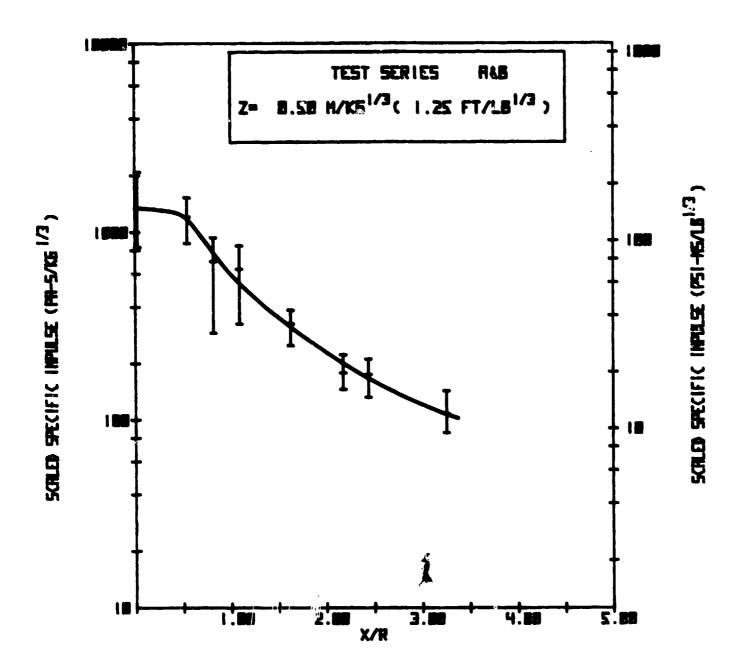


FIGURE 15. SPECIFIC IMPULSE FOR SINGLE CHARGE TESTS (CONT'D)

FIGURE 15. SPECIFIC IMPULSE FOR SINGLE CHARGE TESTS (CONT'D)

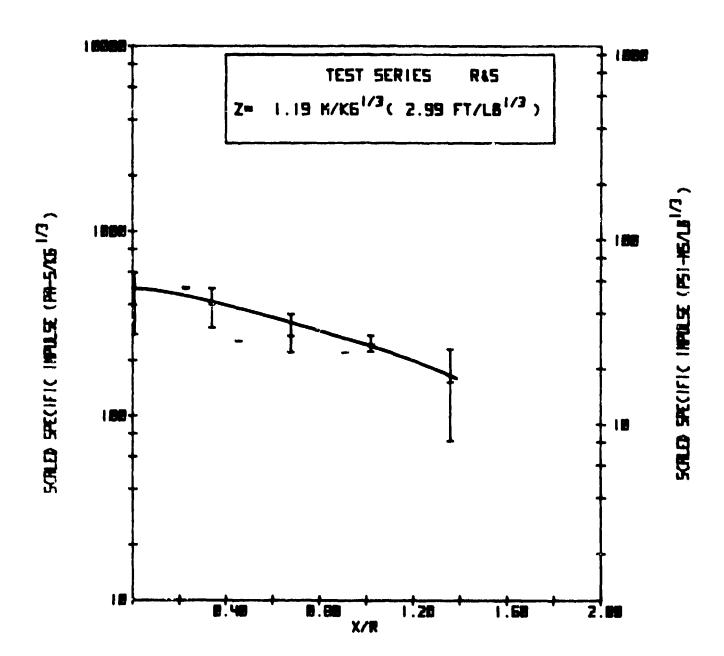


FIGURE 15. SPECIFIC IMPULSE FOR SINGLE CHARGE TESTS (CONT'D)

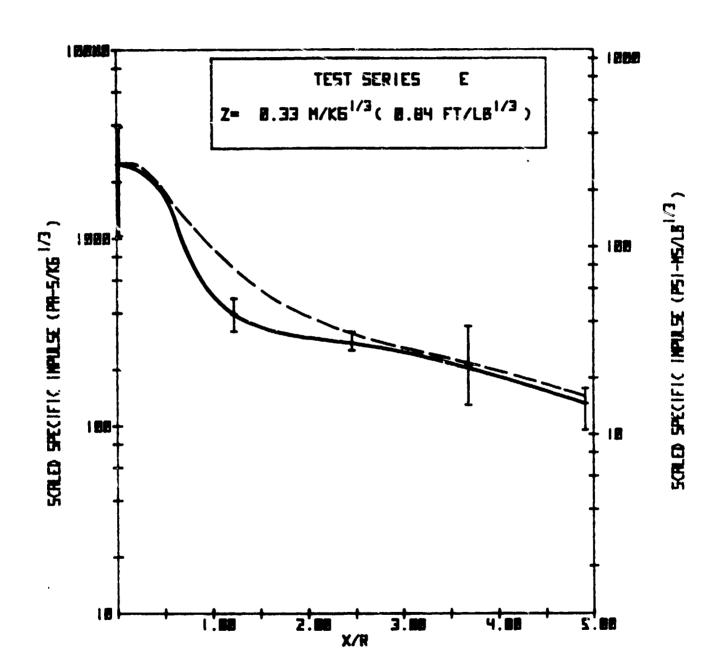


FIGURE 16. SPECIFIC IMPULSE FOR GROUPED ARRAY TESTS

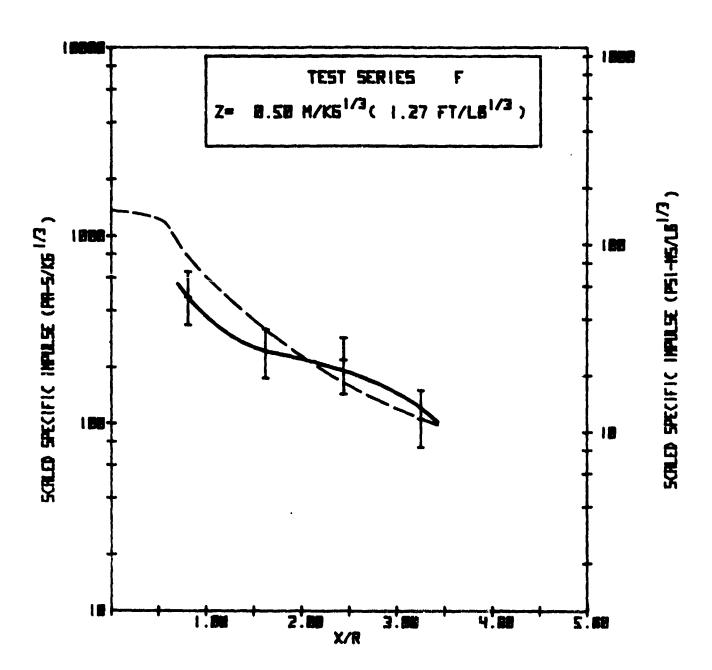


FIGURE 16. SPECIFIC IMPULSE FOR GROUPED ARRAY TESTS (CONT'D)

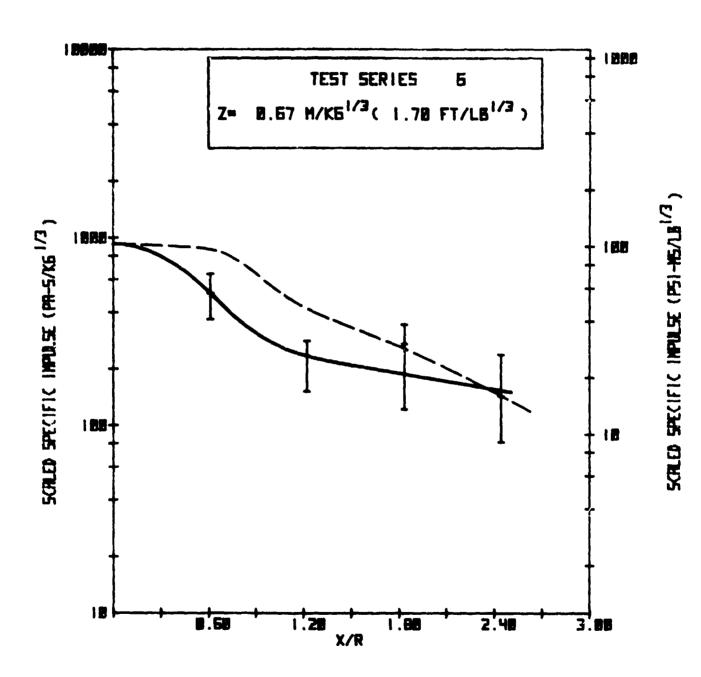


FIGURE 16. SPECIFIC IMPULSE FOR GROUPED ARRAY TESTS (CONT'D)

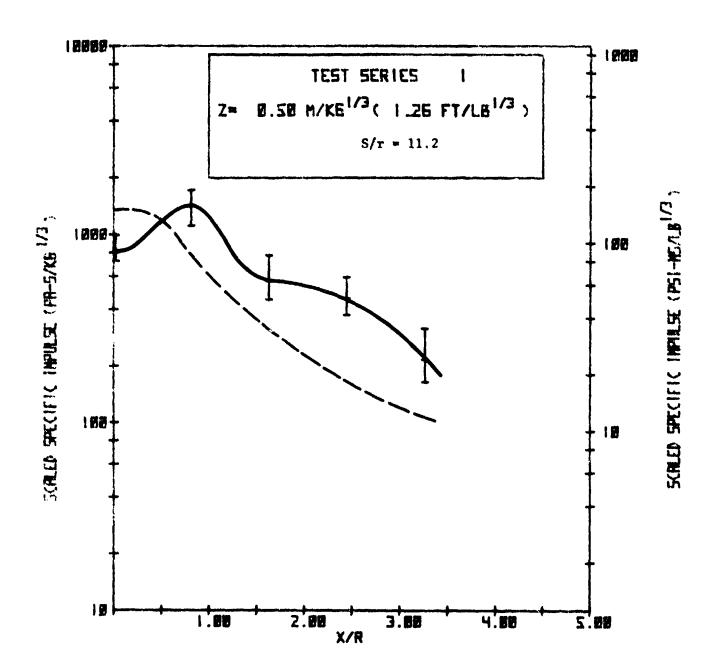


FIGURE 17. SPECIFIC IMPULSE VARIATIONS DUE TO CHARGE STANDOFF FOR HORIZONTAL ARRAY TESTS

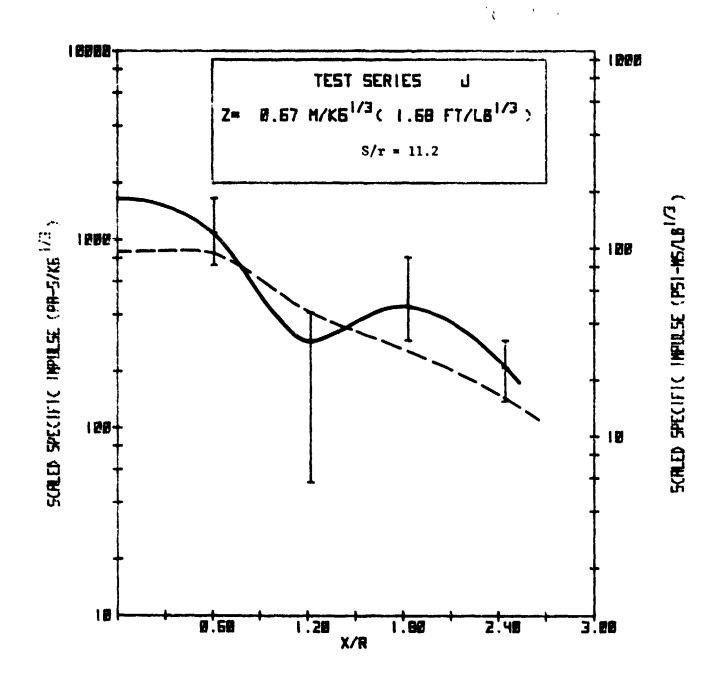


FIGURE 17. SPECIFIC IMPULSE VARIATIONS DUE TO CHARGE STANDOFF FOR HORIZONTAL ARRAY TESTS (CONT'D)

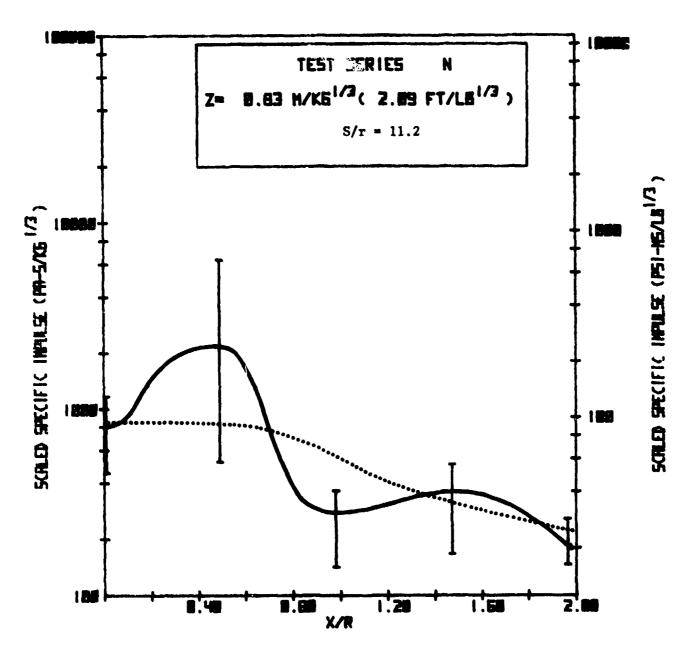


FIGURE 17. SPECIFIC IMPULSE VARIATIONS DUE TO CHARGE STANDOFF FOR HORIZONTAL ARRAY TESTS (CONT'D)

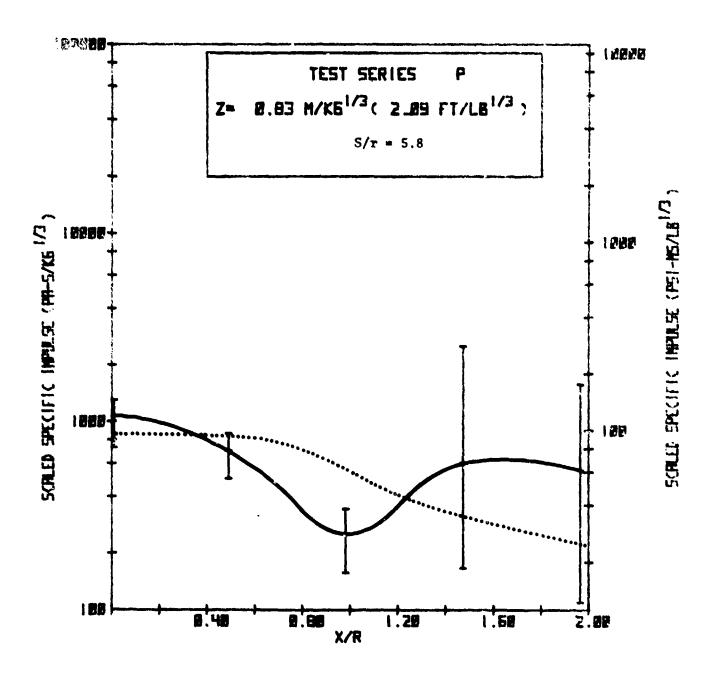


FIGURE 18. SPECIFIC IMPULSE VARIATIONS DUE TO CHARGE SPACING FOR HORIZONTAL ARRAY TESTS (CONT'D)

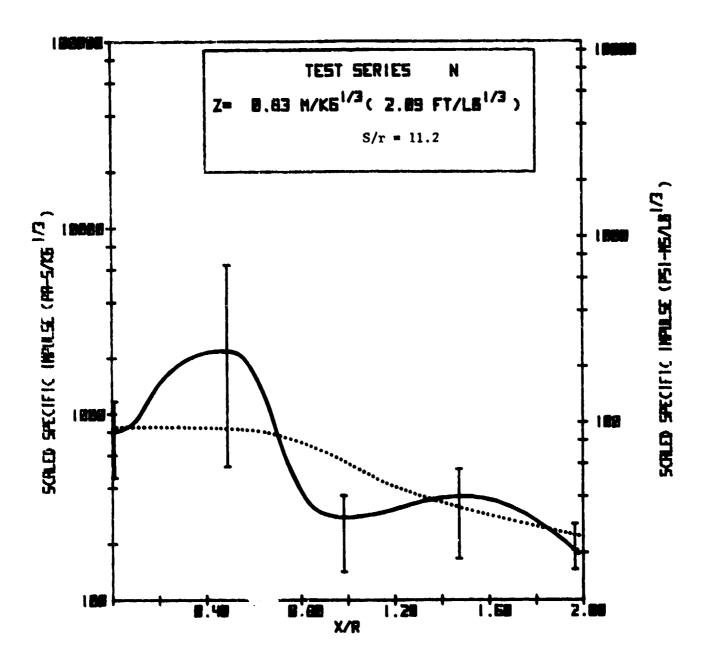


FIGURE 18. SPECIFIC IMPULSE VARIATIONS DUE TO CHARGE SPACING FOR HORIZONTAL ARRAY TESTS (CONT'D)

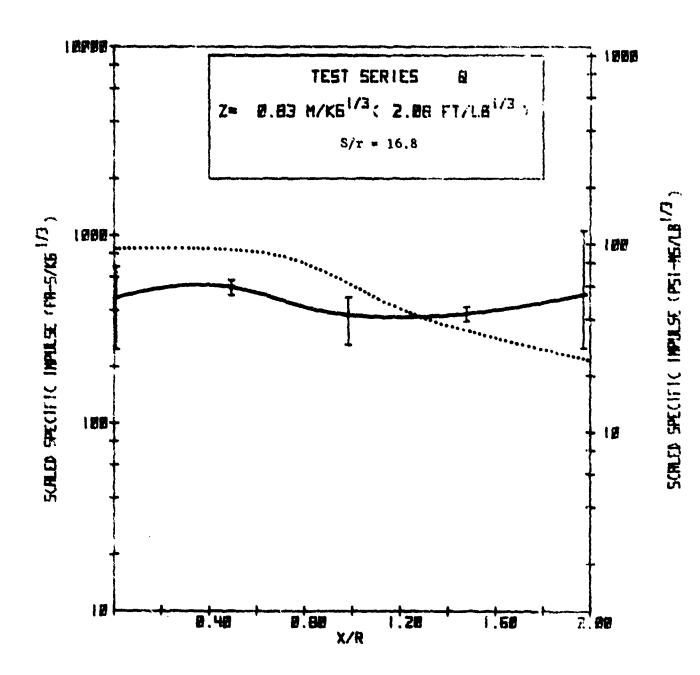


FIGURE 18. SPECIFIC IMPULSE VARIATIONS DUE TO CHARGE SPACING FOR HORIZONTAL ARRAY TESTS (CONT'D)

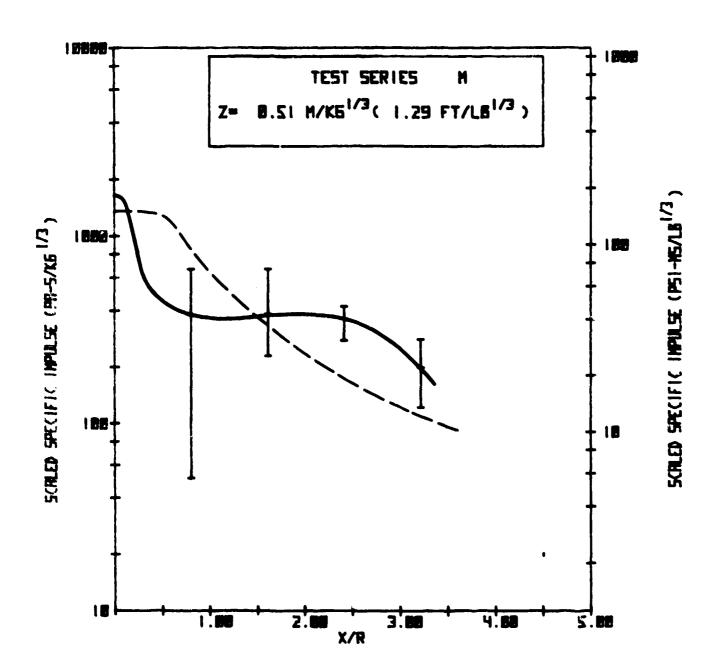


FIGURE 19. SPECIFIC IMPULSE FOR VERTICAL ARRAY TESTS

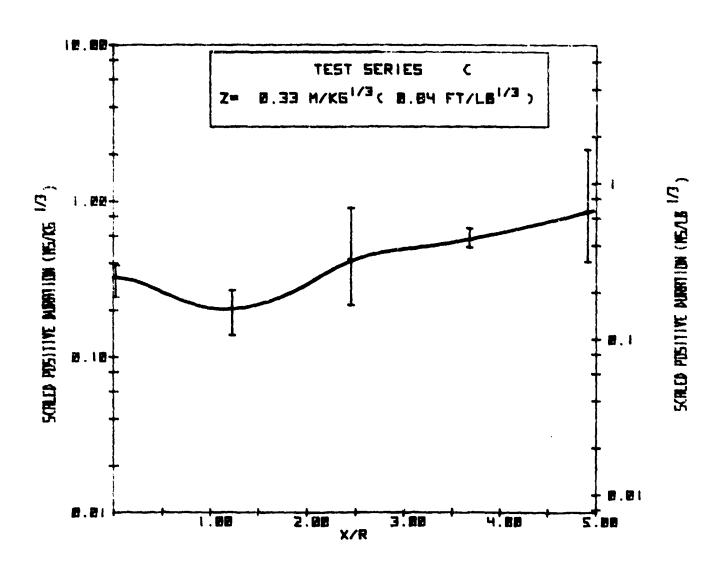


FIGURE 20. POSITIVE DURATION FOR SINGLE CHARGE TESTS

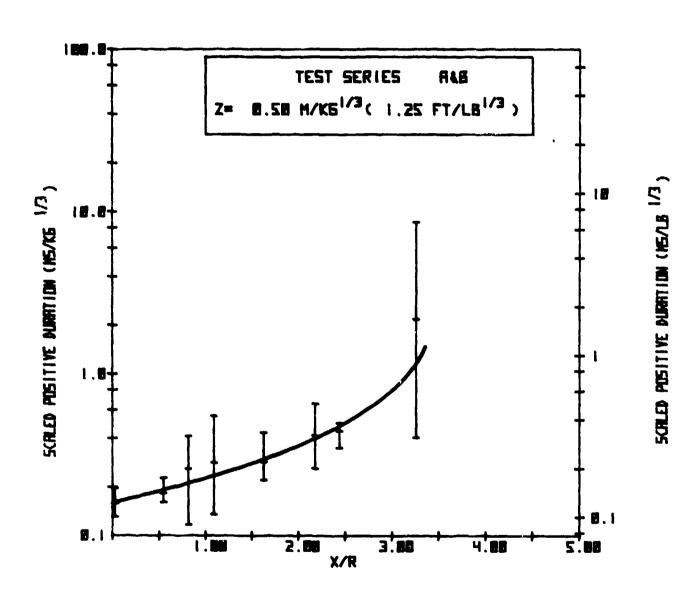


FIGURE 20. POSITIVE DURATION FOR SINGLE CHARGE TESTS (CONT'D)

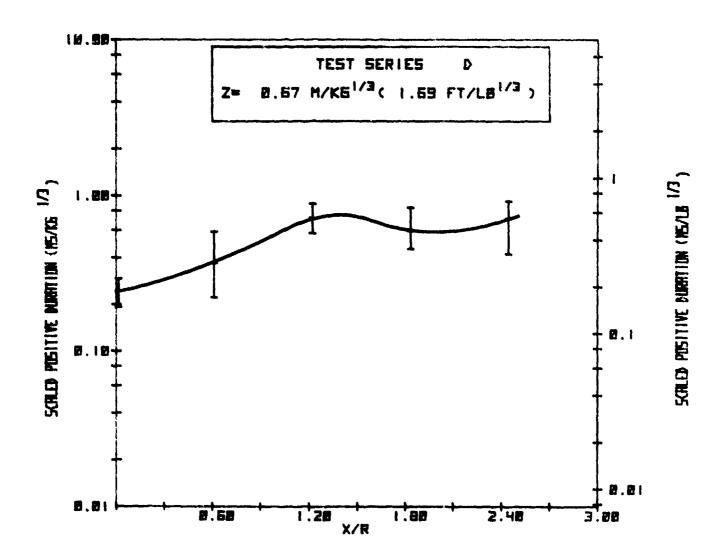


FIGURE 20. POSITIVE DURATION FOR SINGLE CHARGE TESTS (CONT'D)

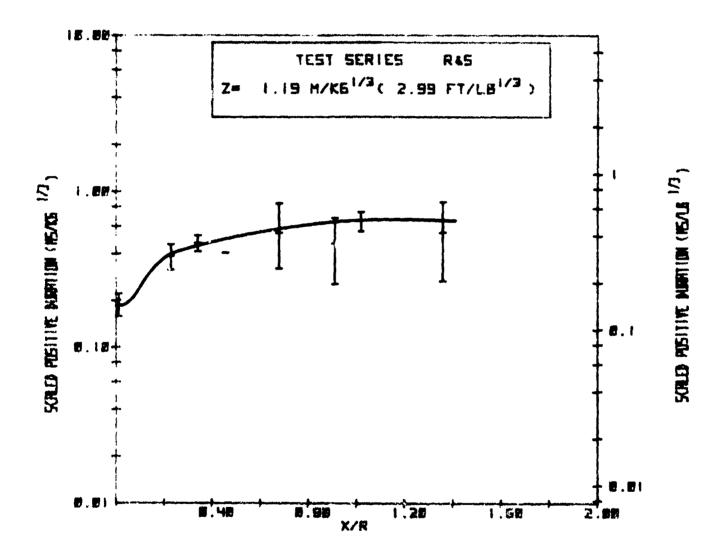


FIGURE 20. POSITIVE DURATION FOR SINGLE CHARGE TESTS (CONT'D)

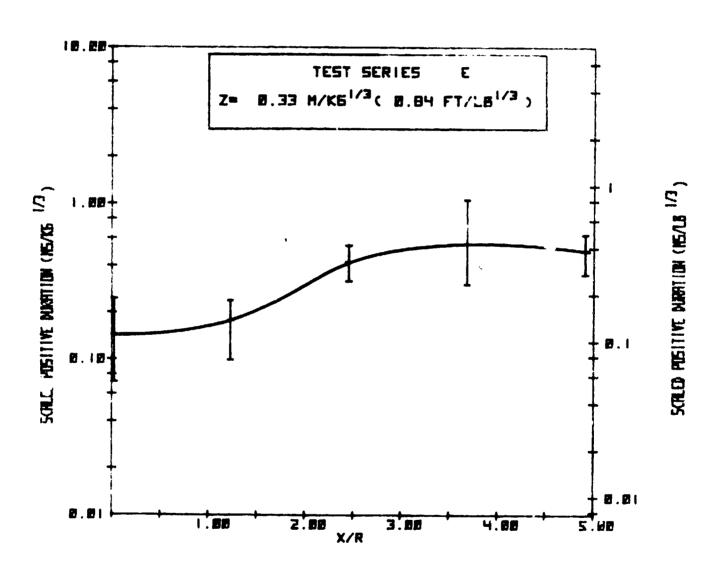


FIGURE 21. POSITIVE DURATION FOR GROUPED ARRAY TESTS

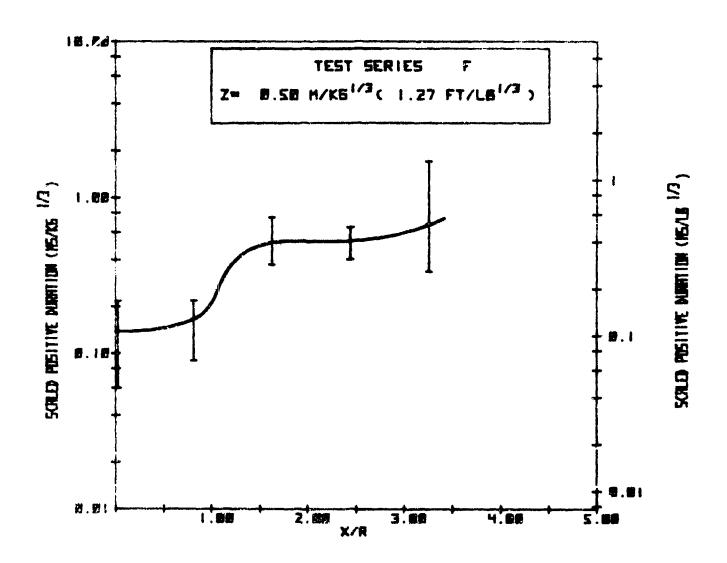


FIGURE 21. POSITIVE DURATION FOR GROUPED ARRAY TESTS (CONT'D)

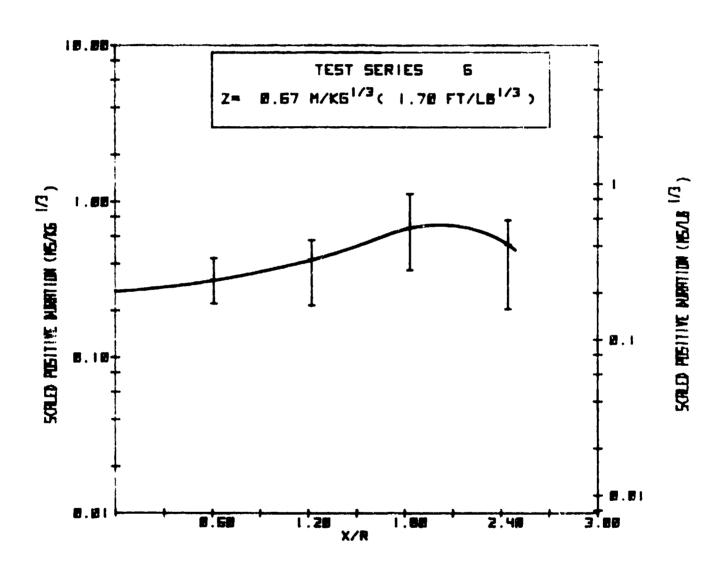


FIGURE 21. POSITIVE DURATION FOR GROUPED ARRAY TESTS (CONT'D)

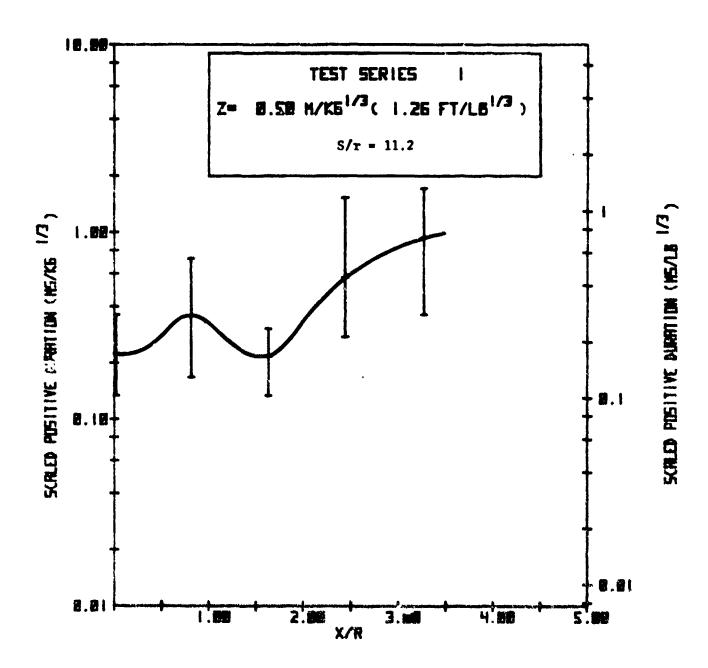


FIGURE 22. POSITIVE DURATION VARIATIONS DUE TO CHARGE STANDOFF FOR HORIZONTAL ARRAY TESTS

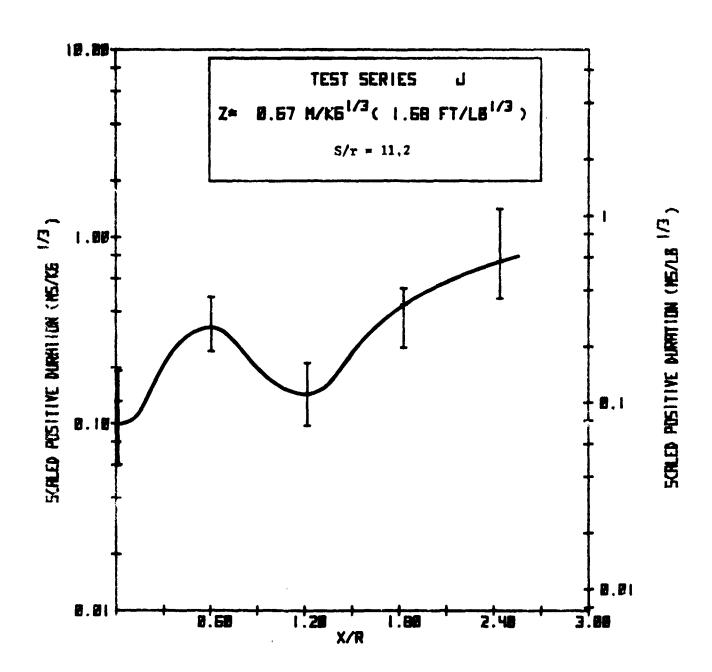


FIGURE 22. POSITIVE DURATION VARIATIONS DUE TO CHARGE STANDOFF FOR HORIZONTAL ARRAY TESTS (CONT'D)

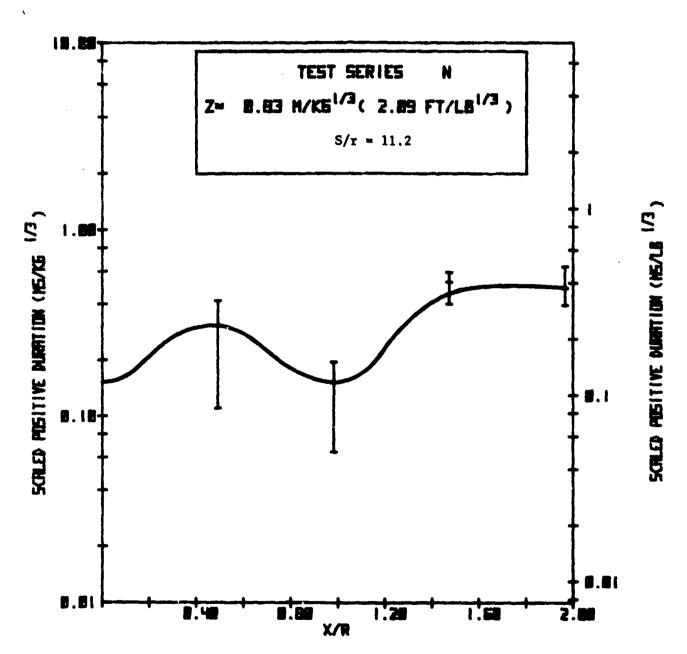


FIGURE 22. POSITIVE DURATION VARIATIONS DUE TO CHARGE STANDOFF FOR HORIZONTAL ARRAY TESTS(CONT'D)

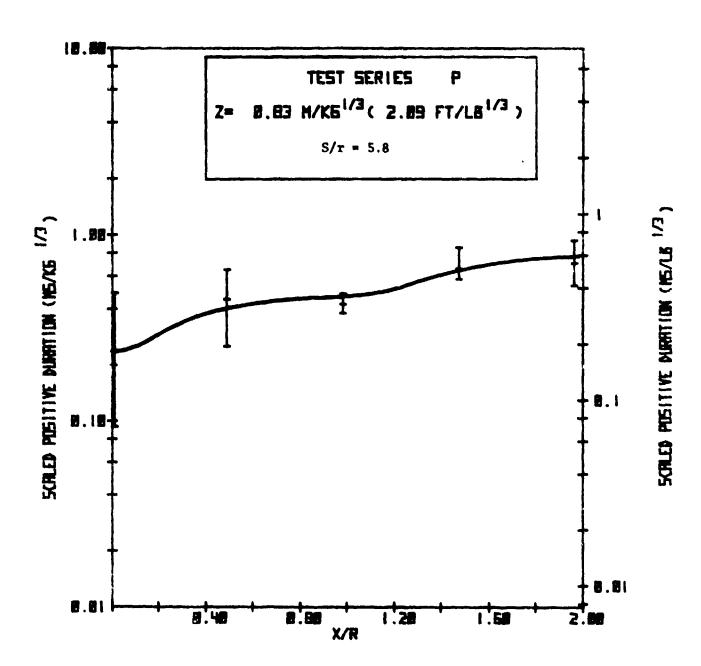


FIGURE 23. POSITIVE DURATION VARIATIONS DUE TO CHARGE SPACING FOR HORIZOUTAL ARRAY TESTS

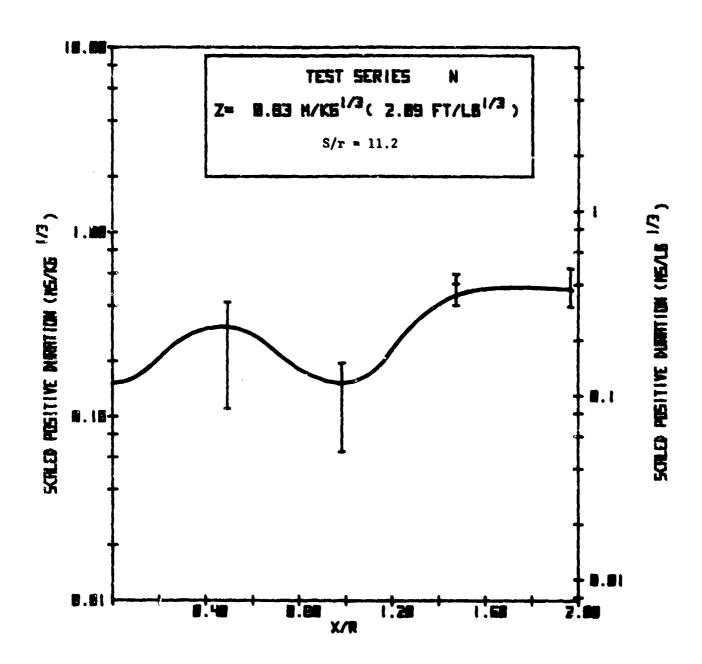


FIGURE 23. POSITIVE DURATION VARIATIONS DUE TO CHARGE SPACING FOR HORIZONTAL ARRAY TESTS (CONT'D)

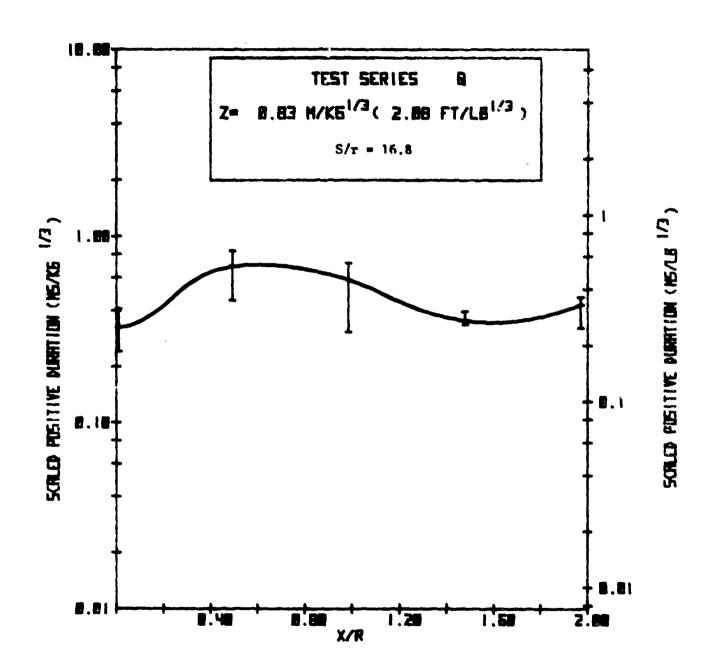


FIGURE 23. POSITIVE DURATION VARIATIONS DUE TO CHARGE SPACING FOR HORIZONTAL ARRAY TESTS (CONT'D)

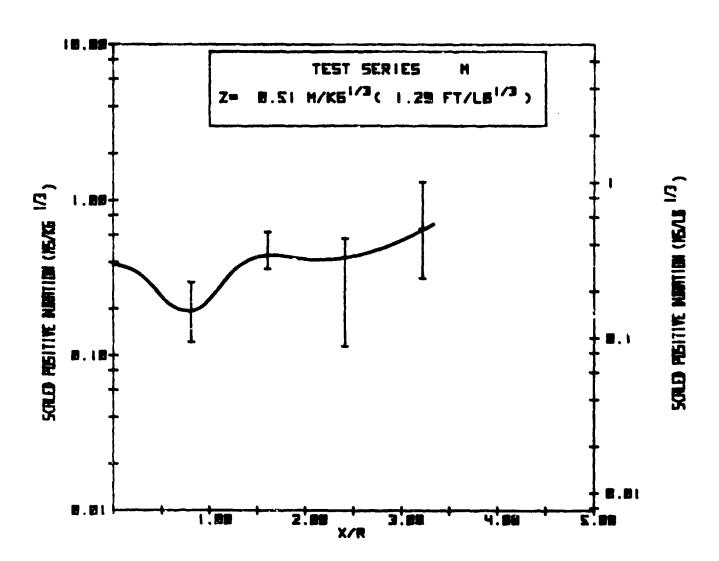


FIGURE 24. POSITIVE DURATION FOR VERTICAL ARRAY TESTS

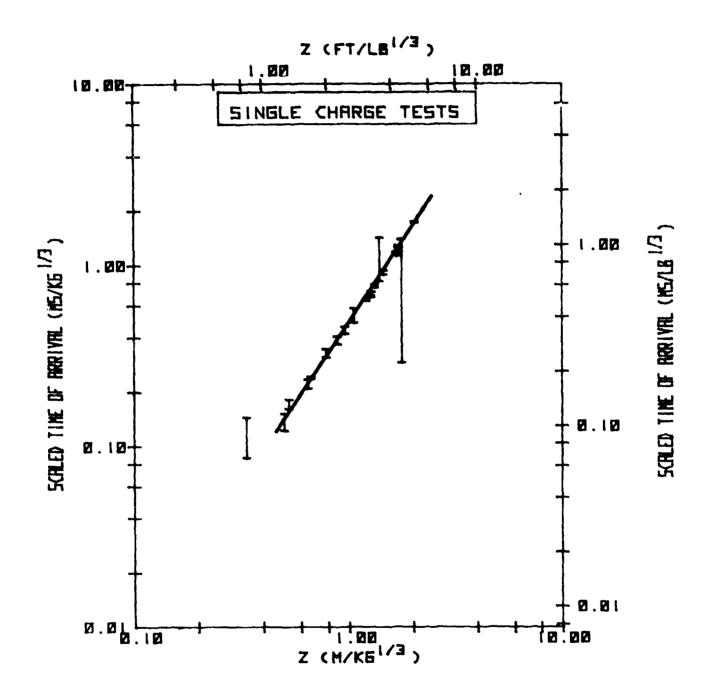


FIGURE 25a. ARRIVAL TIME OF INITIAL SHOCK FRONT FOR A SINGLE CHARGE TESTS

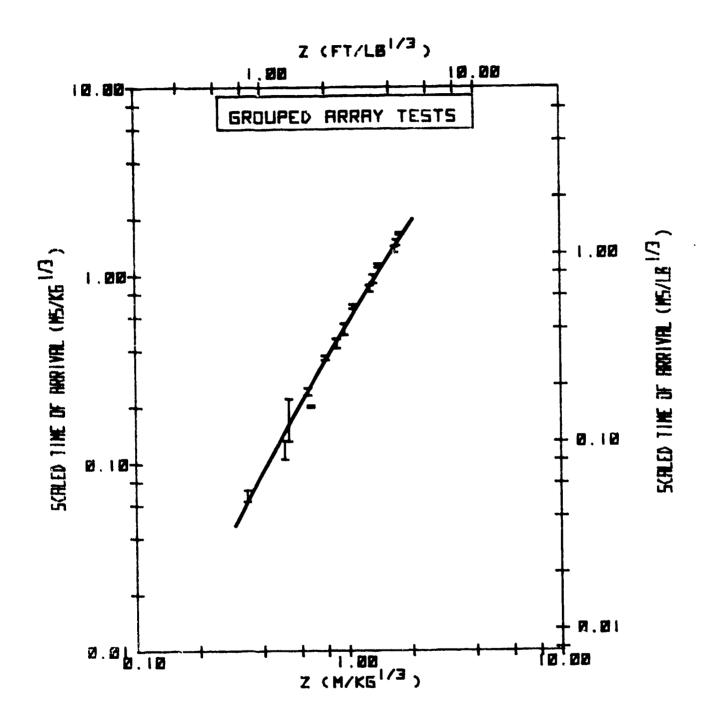


FIGURE 25b. ARRIVAL TIME OF INITIAL SHOCK FRONT FOR A GROUPED ARRAY TESTS

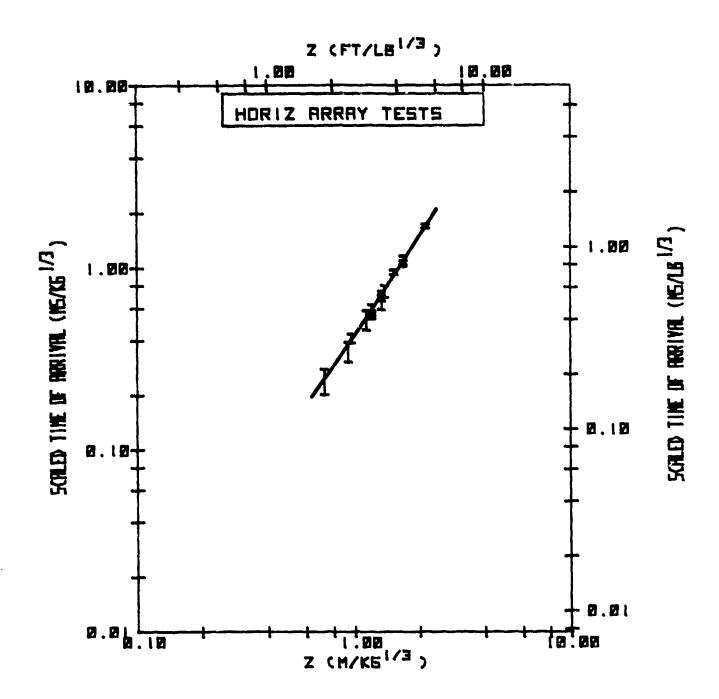


FIGURE 25c. ARRIVAL TIME OF INITIAL SHOCK FRONT FOR A HORIZONTAL ARRAY TESTS

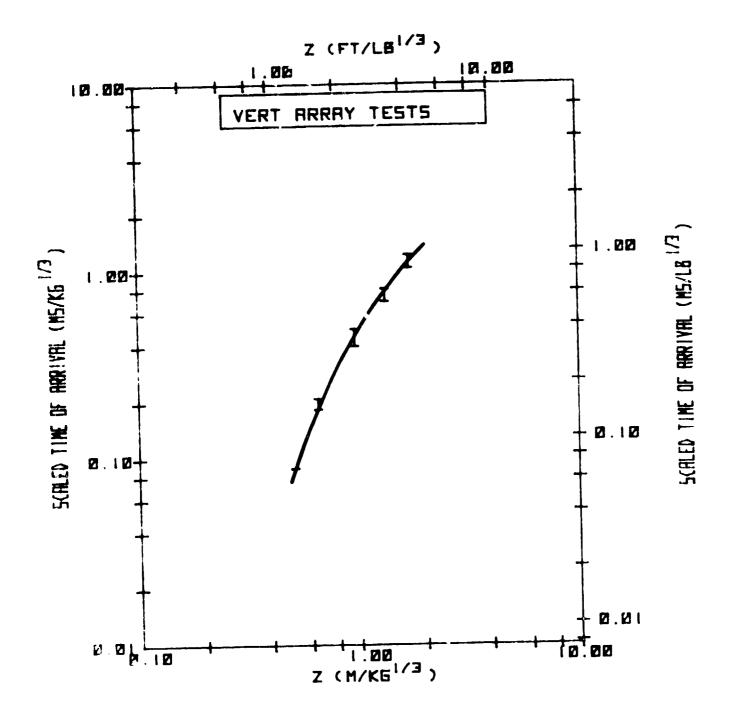
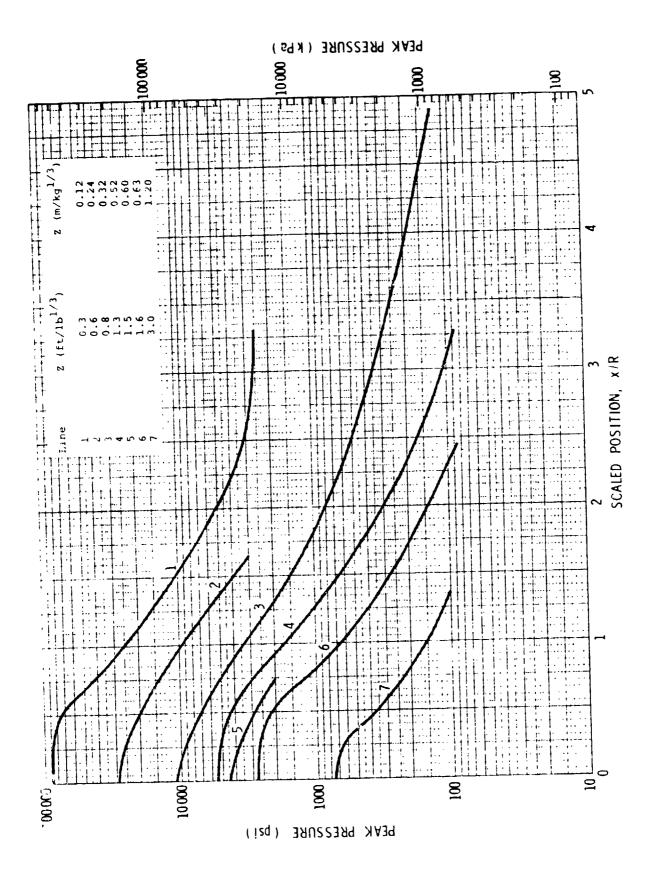


FIGURE 25d. ARRIVAL TIME OF INITIAL SHOCK FRONT FOR A VERTICAL ARRAY TESTS



PEAK PRESSURE US SCALED POSITION FOR DIFFERENT SCALED DISTANCES

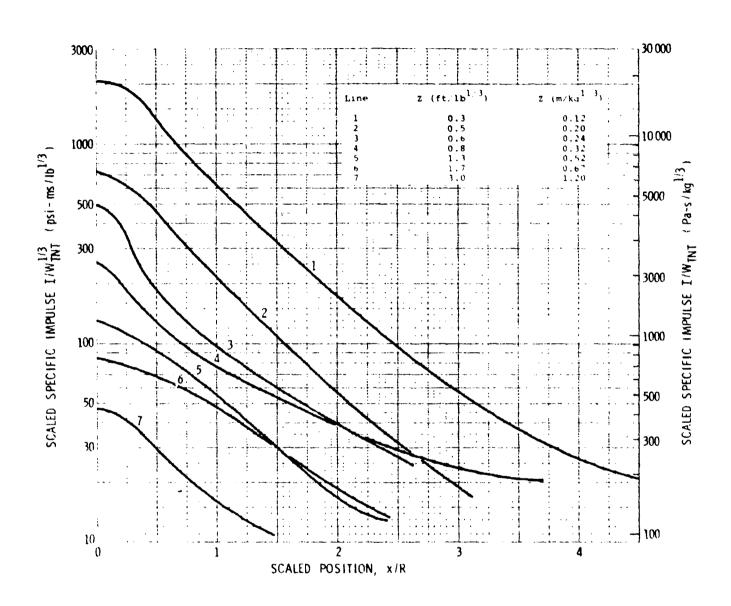


FIGURE 27. SCALED SPECIFIC IMPULSE VS SCALED POSITION FOR DIFFERENT SCALED DISTANCES

Table 1. List of symbols

Symbol .	Definition	Units
E	Energy released by the explosive	FL
r	Radius of charge	L
$\gamma_{f e}$	Explosive products specific heat ratio	-
ρ _e	Density of explosive	FT ² /L ⁴
a _e	Explosive detonation velocity	t./T
g	Effective limit for explosive detonation	L
P _a	Ambient air pressure	F/L^2
a a	Sonic velocity in air	L/T
$\rho_{\mathbf{a}}$	Ambient air density	$\mathrm{FT}^2/\mathrm{L}^4$
$\theta_{f a}$	Ambient air temperature	θ
Υa	Specific heat ratio of air	~
S	Specific entropy	$L^2/T^2\theta$
$v_{\underline{i}}$	Shock velocity	L/T
$ ho_{f s}$	Gas density in shock wave	$\mathrm{FT}^2/\mathrm{L}^4$
u _s	Particle velocity in shock wave	L/T
$\theta_{\mathbf{s}}$	Shock front temperature	θ.
R	Standoff distance	L
$\mathbf{s}_{\mathbf{i}}$	Charge spacing	L
Ф	Shock front encounter angle	_
P	Pressure	F/L^2
I	Specific Impulse	ft/l ²
t	Time	T
t _a	Arrival time of shock wave	T
t _d	Shock wave duration	Ψ

$$\pi_2 = s_1/R$$

$$\pi_2 = g/R$$

$$\tau_{\dot{a}} = \rho_{a}/\rho_{a}$$

$$\pi_8 - U_i/a$$

$$\pi_{10} = 8\theta/a_a^2$$

$$\pi_{12} = R \left(\frac{a_A^2 - \rho_A}{B} \right)$$

$$w_{13} = \rho_{e}/\rho_{e}$$

$$\pi_{14} = \theta_s/\theta_a$$

$$w_{16} = \frac{P R^3}{E}$$

$$\pi_{17} = \frac{I_{\bullet}}{\left(\mathbb{E} \ \mathbb{P}^{2}_{\bullet}\right)^{1/3}}$$

$$p = 1/3$$

$$t_{10} = t_{10} \left(\frac{a}{a} \right)$$

$$\tau_{19} = t_d a_a \left(\frac{P_a}{E}\right)^{1/3}$$

geometric similarity

similar explosives

kinematic similarity

similar atmospheres

modified Sach's scaling

similar shocks

scaled pressure

scaled impulse (

scaled time

TABLE 3.
REPLICA SCALING LAW FOR MULTIPLE DETONATIONS

Quantity	Symbol	Scale Factor
Length	r, s _i , g, R	λ
Impulse	I	λ
Time	t, t _d , t _a	λ
Velocity	U ₁ , u _s , a _s	1.0
Specific He	γ_a , γ_e	1.0
Entropy	S	1.0
Density	ρ_a , ρ_e , ρ_s	1.0
Pressure	Pa, Ps	1.0
Temperature	θ_s , θ_a	1.0
Angle	Φ	1.0
Energy	E	λ^3

TABLE 4. TEST PROGRAM

Scaled Standoff $m/\kappa g^{1/3}$ (ft/1b ^{1/3})	0.335 (0.84)	0.504 (1.27)	0.495 (1.25)	0.672 (1.70)	1.21 (3.04)	1.18 (2.99)	0.332 (0.834)	0.499 (1.26)	0.665 (1.68)	0.495 (1.25)	0.665 (1.68)	0.821 (2.07)	0.821 (2.07)	0.821 (2.07)	0.504 (1.27)*
Standoff m (ft)	0.29 (0.95)	0.437 (1.43)	0.652 (2.14)	0.582 (1.91)	1.05 (3.43)	1.56 (5.13)	0.29 (0.95)	0.436 (1.43)	0.582 (1.91)	0.436 (1.43)	0.582 (1.91)	0.724 (2.38)	0.724 (2.38)	0.724 (2.38)	0.437 (1.43)
Charge Separation m (ft)	ı	;	ı	i	ı	ı	0	0	0	0.71 (2.33)	0.71 (2.33)	0.366 (1.2)	0.71 (2.33)	1.07 (3.5)	0.145 (0.475)
No. Charges	1	1	1	1	7	1	٣	٣	ю	ю	٣	ъ	٣	٣	m
Charge Weight Kg (1b)	0.65 (1.43)	0.65 (1.43)	2.29 (5.05)	0.65 (1.43)	0.65 (1.43)	2.29 (5.05)	0.223 (0.492)	0.223 (0.492)	0.223 (0.492)	0.223 (0.492)	0.223 (0.492)	0.223 (0.492)	0.223 (9.492)	0.223 (0.492)	0.223 (0.492)
No. Shots	m	М	٣	m	2	1	٣	т	т	ю	٣	٣	7	٣	4
Test Series	Н	7	1 .	1	1	1A	2	2	2	٣	က	٣	ю	Э	4
Designation	ပ	¥	Ø	Ω	∝	S	ы	<u>pu</u>	U	ы 82	٦	Ā	Z	ø	×

 * For these tests, R is measured to the center of mass of the charges and W is the total weight of Composition B explosive.

APPENDIX DATA SUMMARIES

Table A.1 Metric Unit Summary

Single Charge Tests Grouped Array Tests Horizontal Array Tests Vertical Array Tests

Table A.2 English Unit Summary

Single Charge Tests Grouped Array Tests Horizontal Array Tests Vertical Array Tests TABLE A.1 METRIC UNIT SUMMARY

SUMMARY OF SINGLE CHARGE TEST DATA

TIME OF ARRIVAL (MS)	1.073	0.655	0.384	0.203	0.125	0.197	0.398	0.682	1.098	1.039	0.655	0.363	0.181	0.106	0.186	0.379	0.670	1.073	1.039	0.660	0.382	0.195	0.131	0.193	0.386	0.673	000.0	0.801	0.521	0.361	7 10	671.0	0.196	0.547	0.527	0.788	0.788	0.499	0.313	0.188	0.202	0.331	0.499	.76
POSITIVE DURATION (MS)	0.437	0.379	0.203	0.236	000.0	0000	000.0	000.0	0.749	•	0.432	0.192	0.357	0.129	0.101	0.376	0.303	7.487	0.351	0.393	0.277	0.246	0.113	0.180	0.211	0.418	000.0	0.381	0.378	0.722	0.210	0.260	0.300	0.203	٠	•	0.482	0.320	0.442	0.250	0.212	•	0.382	0.862
POSITIVE IMPULSE (PA-S)	999,	0.0	328.5	624.9	995.1	251.8	233.0	170.7	123.1	89.3	138.9	215.1	627.9	1107.3	614.5	262.8	114.0	0.0	73.7	146.4	320.6	664.5	718.5	806.0	273.0	181.9	0.0	232.4	378.3	499.7	1147.0	2.05/2	14/6.3	426.7	452.7	191.0	234.1	394.4	0.989	1503.6	2007.1	834.7	504.2	233.5
PEAK PRESSURE (KPA)	617.8	1232.8	4596.7	17141.0	31719.3	20627.0	4884.2	932.2	623.3	601.2	1167.3	2558.0	8994.2	13652.3	21006.2	2453.8	1354.8	550.9	643.6	1909.9	4003.6	14434.9	18837.3	17065.4	4548.5	1507.0	0.0	1675.0	٠	10433.9	29913.5	62001.0	3225/.4	9571.4	4641.6	1576.2	1665.4	3197.9	4904.0	22594.8	27036.8	12541.9	4019.4	_
CHARGE SPACING (M)	0.000	00000	0000	000.0	0.000	000.0	•	0000	0.000	000.0	•	0000	000.0	000.0	0.000	000.0	0000	0.00	0000	0.000	0000	0.00	•	0.00	00000	000.0	000.0	٠	•	•	0.000	٠	•	٠	٠	٠	000.0	000.0	0.000	00000	•	00000	00000	0.000
GAGE LOCATION (M)	-1.443	-1.082	-0.721	-0.361	00000	0.361	0.721	1.082	1.443	-1.443	-1.082	-0.721	-0.361	0000	0.361	0.721	1.082	1.443	-1.443	-1.082	-0.721	-0.361	0000	0.361	0.721	1.082	1.443	-1.443	-1.082	-0.721	-0.361	000.0	0.361	0.721	1.082	1.443	-1,443	-1.082	-0.721	-0.361	0,361	0.721	1.082	1.443
GAGE	*	7	ליו	4	'n	9	7	œ	٥		2	ю	4	'n	9	7	0	6	+	7	ליו	4	ហ	9	7	80	0	-	7	ימו	4 1	. را	•	7	60	٥		7	m	4	•		. 00	٥
STANDOFF DISTANCE (M)	0.437	0.437	4	.43	43	. 43	0.437	4	4	4	43	. 43	4.	4	4	0.437	4	0.437	4	4	4	0.437	4	4.	4	4	4.	á	•	d)	٠		٠	•	•	0.653	•	9	9	.65	•	65	1.00	0.653
CHARGE UEIGHT (KG)	0.649	0.649	•	.64	.64	٠		.64		•		ó	0.649	9	4	•		•	•	6	0.649		9	9	6	ó	•	Ġ	2.291	ú	٠	٠	•	•	•	•	Ġ	Ġ	Ú	Ġ	5			29
TEST ID	1.0	14	14	14	4	18	18	14	14	28	2 A	2 A	2₽	2 A	2₽	2₩	24	2₽	34	34	3♠	3.4	3A	3A	36	3A	3A	20B	20 8	20B	208	20B	20B	20B	30E	20B	21B	21B	218	218	218	218	218	218

TIME OF ARRIVAL (MS)	0.752	0.196	0.183	٠	0.497	100	٠	• •	0.146	980.0	0.154	0.332	0.615	0.000	0.982	0.590	0.328	0.149	0.075	0.140	0.352	0.620	1.023	1.0.0	0.611	0.331	0.158	0.125	0.145	0.332	0.611	000.0	1.211	0.781	0.473	0.270	0.276	49	0.711	1.213	0000
POSITIVE DURATION (HS)	0.344 0.318	0.225	•	•	0.469	0.731	0.530	•	0.196	0.211	0.162	0.187	0.581	0.000	0.384	0.439	0.312	0.209	0.295	0.233	•	0.518	1.863	0.383	0.505	•	٠	0.336	0.119	•	0.456	0.00	0.00	0.436	0000	0.288	0000		0.728	000	00000
POSITIVE IMPULSE (PA-S)	215.8	1554.2	1839.3	1111.4	505.2	272.6	C•/8	107.	753.9	1539.8	733.1	218.9	169.4	0.0	116.4	180.5	276.5	551.3	2003.8	527.4	338.3	224.5	159.0	115.1	186.1	303.5	346.6	2848.9	558.5	249.6	209.8	0.0	112.2	181.6	346.8	783.2	829.3	295.8	252.6	136.6	0.0
PEAK PRESSURE (KPA)	1655,9	33401.0	35590.0	15786.9	4149.1	6.0//1	728.3	C'9771	14416.9	77684.6	15231.0	3335.8	1460.4	0.0	867.8	1962.0	3735.1	15312.0	77273.6	26805.9	4362.4	1764.6	971.4	8.988	1774.1	3301.4	8833.9	77421.9	18000.7	3467.4	1924.4	0.0	571.2	1605.1	2330.4	12089.7	13382.1	3192.7	1660.9	626.0	
CHARGE SPACING (M)	00000	000.0	000.0	000.0	00000	000.0	0000	0000	000	00000	0000	0000	00000	00000	000.0	0000	00000	00000	00000	0000	00000	0.000	00000	0000	00000	00000	0000	0000	000.0	000.0	000.0	000.0	0000	0000	00000	0000	00000	•	00000	000.0	00000
GAGE LOCATION (M)	-1.082	-0.361	0.361	0.721	1.082	1.443	-1.443	780.1-	-0.361	000.0	0.361	0.721	1.082	1.443	-1.443	-1.082	-0.721	-0.361	00000	0.361	0.721	1.082	1.443	-1.443	-1,082	-0.721	-0.361	0.000	0.361	0.721	1.082	1.443	-1.443	-1.082	-0.721	-0.361	0,361	0.721	1.082	1.443	
GAGE NO	- 7	n 4	• •0	^	00	۰ ۰	(N 1	ว ◀	· W7	۰ م	^	100	•	-4	7	м	4	N O	•	7	œ	٥.	-	7	m	*	ID.	•	7	œ	٥	-	7	м	4	•9	7	. 00	0	· ••4
STANDOFF DISTANCE (M)	0.653	0.653	0.653	0.653	0.653	0.653	0.290	0.240	0.250	0.290	0.290	0.290	0.290	0.290	0.290	0.290	0.290	0.290	0.290	0.290	0.290	0.290	0.290	0.290	0.290	0.290	0.290	0.290	0.290	0.290	0.290	0.290	0.582	0.582	0.582	0.582	0.582	0.582	0.532	0.582	•
CHARGE WEIGHT (KG)	2.291	2.291	2.291	2.291	2.291	٠	•	0.649	0.044	0.649		0.649	0.649	0.649	0.649	0.649	0.649	0.649	0.649	0.649	0.649	0.649	0.649	0.649	0.649	0.649	0.649	0.649	0.649	0.649	0.649	0.649	0.649	0.649	0.649	0.649	0.649	0.649	0.649	0.649	9
TEST ID	22B 22B	22B 22B	22B	22B	22B	22B	75	2,5	2 %	70	20	20	20	20	ည္တ	36	90	36	90	3 6	38	8 C	90	<u>ئ</u> ر	26	90	3 6	26	<u>ه</u>	36	26	26	40	40	40	40	40	40	4	E	និ

SUMMARY OF SINGLE CHARGE TEST DATA

TIME OF ARRIVAL (MS)	1.231	0.501	0.298	0.210	•	0.468	0.751	7	1.140	0.742	0.419	0.272	0.205	0.274	0.473	0.778	0.251	1.510	.118	J.813	0.621	0.560	0.623	0.813	1.111	1.489	1.514	1.095	0.773	0.592	0.553	0.592	0.778	٠	1.508	٠	1.190	000.0	0.865	0.037	0.870	966.0	1.213	49
POSITIVE DURATION (HS)	0.395	0.640	0.508	0.254	0.192	0.582	0.674	0.691	0.366	0.414	0.768	0.377	0.166	0.236	0.499	0.449	0.793	0.232	0.575	0.731	0.428	0.152	0.360	0.311	0.585	0.745	0.357	0.483	0.648	0.456	0.137	0.389	0.405	0.642	0.566	0.337	0.424	0.000	909.0	0.291	0.417	0.537	0.689	968.0
POSITIVE IMPULSE (PA-S)	314.4	248.2	811.6	602.0	618.0	323.3	257.6	151.8	93.4	165.3	551.6	9.029	717.2	798.8	354.2	170.2	128.1	62.9	201.1	308.2	374.4	512.5	260.6	191.7	192.4	198.8	82.7	214.6	202.7	424.0	238.6	334.4	258.6	235.6	180.1	0.0	313.7	0.0	642.6	783.8	654.3	334.9	- (1)	90.
PEAK PRESSURE (KPA)	1970.9	2832.7	11734.0	17335.2	14248.4	3531.2	1840.0	288.6	664.1	1208.4	2073.7	13604.1	19811.6	12073.1	3621.5	1509.4	556.2	711.1	1297.7	2220.8	4521.1	0.0	3701.6	1411.7	1318.6	788.3	558.9	1299.5	1322.4	4604.9	4385.8	4783.6	1681.4	1291.2	764.4	0.0	1674.3	0.0	5635,9	7927.7	4368.7	2606.2	2040.7	1057.6
CHARGE SPACING (M)	0.000	00000	000.0	٠	0000	0000	•	0000	00000	000.0	0.000	00000	0000	00000	0000	000.0	0.000	00000	00000	00000	0000	•	0000	•	00000	0000	000.0	•	000.0	•	٠	٠	٠	•	•	00000	•	000.0	0000	000.0	00000	00000	0.000	•
GAGE LOCATION (M)	-1.082	-0.721	-0.361	000.0	0.361	0.721	1.082	1.443	-1.443	-1.082	-0.721	-0.361	0000	0.361	0.721	1.082	1,443	-1,443	-1.082	-0.721	-0.361	00000	0.361	0.721	1,082	1.443	-1.443	-1.082	-0.721	-0.361	0000	0.361	0.721	1.082	1.443	-1,443	-1.082	-0.721	-0.361	00000	0.361	0.721	1.082	1.443
GAGE NO	7	173	4	N)	9	7	80	٥	7	7	м	4	U	9	7	80	٥	-	7	ы	4	ŀΩ	9	7	80	٥٠	-	7	м	4	ហ	9	7	30	D.	-	2	ю	4	מו	9	7	60	6
STANDOFF DISTANCE (M)	0.582	•	•	•	0.582	0.582	0.582	0.582	0.582	0.582	0.582	0.582	0.582	0.582	0,582	0.582	0.582	1.046	•	1.046	1.046	1.046	1.046	1.046	1.046	1.046	1.046	1.046	1.046	٠	1.046	٠	٠	•	1.046	1.562	1.562	1.562	1.562	1.562	1.562	•	1.562	
CHARGE WEIGHT (KG)	0.649	0.649	0.649	0.649	0.649	0.649	0.649	0.649	•	0.649	0.649	0.649	•	0.649	0.649	0.649	0.649	•	0.649	0.649	0.649	0.649	0.649	9	0.649	•	0.649	0.649	0.649	•	0.649	٠	0.649	٠	•	2.271	•	2.291	2.291	٠	2.291	2.291	2.291	2,291
TEST Iñ	20	20	SD	รถ	a a	50	50	ฉฉ	4 0	90	90	Q9	9	9	90	90	6 D	38R	38R	38R	38R	3 8K	38K	3CR	38K	33R	40R	40K	40K	40R	408	4 ₹	4 2 3	4 0R	4 0R	395	395	395	375	390	368	393	37.5	392

TIME OF ARRIVAL (MS)		1.147	2 . C	505.0	0.000	0.054	0.114	0.356	0000	1.145	1.145	0.716	0.384	0.150	0.062	0.161	0.394	0.765	1.229	1.183	000.0	0.398	0.191	0.059	0.145	0.368	1,153	1.247	0.784	0.449	0.210	000.0	0.200	0.478	0.848	1.338	1.268	0.833	0.418	0,215	0.208	0.470		0.869
POSITIVE DURATION (MS)		0.305	0.310	204.0	0000	0.062	0.160	0.462	0000	0.433	0.358	0.264	0.299	0.160	0.213	980.0	0.469	0.917	0.440	0.030	000.0	0.276	0.207	960.0	0.152	0.295	0.531	0.291	0.421	0.556	0.174	000.0	0.190	0.649	0.518	0.460	0.380	0.488	•		0.174	151		0.562
POSITIVE IMPULSE (PA-S)		82.0	1111.7	0.0	276.5	0.0	0.0	236.0	0.0	109.7	122.7	137.9	218.6	380.6	3388.8	293.0	235.2	293.7	119.3	111.7	0.0	273.9	0.0	880.8	413.7	234.4	136.5	65.2	151.7	219.2	395.2	0.0	557.8	275.8	220.6	89.6	75.8	168.2	201.3	524.7	289.4	188.1		247.4
PEAK PRESSURE (KPA)		623.7	1148.0	1361.1	0.0	51715.2	5650.9	1874.3	0.0	697.0	678.0	1036.2	2857.3	7144.8	40217.8	8241.0	1543.2	1045.7	694.2	659.7	0.0	2109.4	0.0	20936.7	10006.8	1948.0	0.0	625.2	1088.6	1997.5	9159.9	0.0	11410.5	1530.4	1010.2	574.3	677.2	922.5	1594.5	11625.4		1727.9		992.1
CHARGE SPACING (M)		0.000	000.0	•	٠	0.000	00000	0000	000.0	00000	000.0	00000	0.000	000.0	0.000	00000	00000	0000	00000	00000	00000	0.00	•	00000	00000	000.0	00000	00000	00000	00000	00000	00000	0.000	00000	00000	00000	000.0	00000	00000	00000	00000	• •		00000
GAGE LOCATION (M)		-1.443	-1.082	-0.721	-0.361	000.0	0.361	0.721	1.082	1,443	-1.443	-1.082	-0.721	-0.361	00000	0.361	0.721	1.082	1.443	-1.443	-1.082	-0.721	-0.361	00000	0.361	0.721	1.443	-1.443	-1.082	-0.721	-0.361	000.0	0.361	0.721	1.082	1,443	-1.443	-1.082	-0.721	-0.361	0.361	0.721		1.082
GAGE	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		7	מי	4	מו	9	7	8	٥	+1	7	m	4	מו	9	7	. 00	• 6	+	7	100	*	SO.	9	7	0-		7	m	*	I)	9	7	80	٥	. ₩	2	110	4	•	۰,		œ
STANDOFF DISTANCE (M)		0.290	0.230	0.290	0.290	0.290	0.290	0.290	0.290	0.290	0.290	0.290	0.290	0.290	0.290	0.290	0.290	0.290	0.290	0.290	0.290	0.290	0.290	0.290		0.290	0.290	0.437	0.437	0.437	0.437	0.437	0.437	0.437	0.437	0.437	0.437	5,437	0.437	0.437	•	0.437		0.437
CHARGE WEIGHT (KG)		0.222	0.222	٠	0.222	•	0.222	0.222	0.222	0.222	0.222	0.222	0.222	0.222	0.222	0.222	0.222	0.222	0.222	0.222	0.222	0.222	0.222	0.222	0.222	0.222	0,222	0.222	0.222	0.222	0.222	0.222	0.222	0.222	0.222	0.222	0.222	0.222	0.222	0.222	0.222			0.222
TEST ID		16E	16E	16E	16E	16E	16E	16E	16E	16E	17E	17E	175	17E	17E	17E	175	17E	17E	182	18E	18E	18E	18E	18E	18E	18E	13F	13F	13F	13F	13F	13F	13F	13F	13F	14F	14F	145	14F	14F	14F	:	14F

SUMMARY OF GROUPED ARRAY TESTS

TIME OF ARRIVAL (MS)	0.841 0.460 0.216	0.218 0.427 0.806 1.284	1.455 0.992 0.594 0.325 0.172	0.307 0.575 0.953 1.420	1.452 0.000 0.578 0.307 0.176	0.9905 0.9905 1.433 1.433 0.995 0.318 0.328 0.988
POSITIVE DURATION (MS)	0.350 0.322 0.078	0.091 0.351 0.421 1.484	0.452 0.972 0.492 0.000	0.273 0.466 0.790 0.661	0.460 0.000 0.406 0.193 0.295	0.400 0.384 0.177 0.316 0.316 0.231 0.251 0.497
POSITIVE IMPULSE (PA-S)	124.1 151.0 355.9	325.7 205.1 220.6 129.6	96.5 283.0 222.5 0.0	376.7 224.8 299.0 114.5	70.5 0.0 510.4 556.6 423.3	243.4 202.1 132.9 133.0 131.0 513.0 190.5 289.6
PEAK PRESSURE (RPA)	1067.6 1763.6 9401.0	9108.4 1719.2 938.4 615.4	492.1 813.2 1322.7 5526.9 17381.8	6703.8 1187.0 890.6 616.0	724.1 0.0 1259.7 5937.0 0.0	2016.9 1110.5 755.7 692.5 1353.0 1484.9 6014.1 8784.3 1424.5 647.7
CHARGE SPACING (M)	000000	00000	000000	000000	000000000000000000000000000000000000000	
GAGE LOCATION (M)	-1.082 -0.721 -0.361	0.361 0.721 1.082 1.443	-1.443 -1.082 -0.721 -0.361	0.351 0.751 1.082 1.443	-1.443 -1.082 -0.721 -0.361 0.000	0.721 1.082 1.443 -1.443 -0.361 0.361 1.082 1.082
GAGE NO	0 W 4	0 N B O	ተሪያ ተሪያ	~ C 80 C	ተሪክ ቀርን 40	てほりまごさみるアロウ
STANDOFF DISTANCE (M)	0.437 0.437 0.437	0.437 0.437 0.437	0.582 0.582 0.582 0.582 0.582	0.582 0.582 0.582	0.582 0.582 0.582 0.582 0.582	00.582 00.582 00.582 00.582 00.582 00.582 00.582
CHARGE WEIGHT (KG)	0.222 0.222 0.222	0.222 0.222 0.222 0.222	000000000000000000000000000000000000000	0.222 0.222 0.222	0.222 0.222 0.222 0.222 0.222	00000000000000000000000000000000000000
TEST ID	15F 15F 15F	21111 12111 12111111111111111111111111	106 106 106 106	106 106 106	116 113 116 116	116 116 126 126 126 126 126 126

TIME OF ARRIVAL (MS)	0.499	0.249	0.164	0.225	0.184	0.251	0.145	0.259	0.532	0.488	0.245	0.161	0.236	0.159	0.229	0.154	0.227	0.478	0.440	0.0	0.154		0.134		707.0	0.141	777.0	0.489	0.632	0.358	000.6	0.324	0.311	000.0	0.355	0.633	0.645	0.376	0.238	0.303	0.258	0.339	0000	0.495	7.00	740.0
POSITIVE DURATION (MS)	0.708	1.340	0.203	0.372	0.317	0.636	0.186	0.422	1.310	0.318	0.348	00000	0.147	0.154	0,259	0.117	0.241	0.500	1.501	•	0.178	0,1,0	0.117		0.232	0.267	0.320	0.560	1.239	0.466	000.0	0.214	9:336	000.0	0.225	0.594	0.418	0.458	0.110	0.223	0.169	0.420	0000	0 410 410		0.411
POSITIVE IMPULSE (PA-S)	143.4	325.5	394.4	1150.1	629.4	1322.4	448.8	517.1	276.0	151.0	346.8	677.1	1027.6	861.8	1491.7	478.5	377.8	195.4	148.1	7. V.Z.	420.0	0.000	708.0		1500.0	536.3	403.	200.3	120.7	275.1	0.0	9.869	1348.6	0.0	322.0	185.5	158.6	254.4	44.8	663.7	1432.5	1439.6	0.0	7 0 7 2	0.0to	1//.6
PEAK PRESSURE (KPA)	1384.5	4567.2	3972.5	29784.0	19829.2	26930.2	20711.7	6140.7	2967.5	1330.5	7848.0	29923.1	28489.0	20663.2	22408.8	20893.3	9632.9	2082.4	1560.4	1,0674	1120101	0.10011	10000	5.00.01	29064.0	16997.9	9.0748	1819.0	1342.6	4796.0	0.0	0.0	16210.1	0.0	6736.5	1554.9	1481.2	4320.3	0.0	15384.0		17025.2		A 2 C A	U.4774	1649.7
CHALGE SPACING (M)	0.724	0.724	0.724	•	0.724	0.724	0.724	0.724	0.724	0.724		0.724	0.724	•		0.724	0.724	0.724	467.0	0.72	405.0	*****	47/-0 402-0	17/10	0.724	0.724	0.724	0.724	0,724	0.724	0.724	0.724	0.724	0.724	0.724	0.724	0.724		72	0.724	1	7.	5	֓֝֓֜֝֓֜֝֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֡֓֓֓֓֓֓֓֓֡֓֓֡֓֡֓֡֓֡֓	47.70	0.724
GAGE LOCATION (M)	-1.443	-1.082	-0.721	-0.361	000.0	0.361	0.721	1.082	1.443	-1.443	-1,082	-0.721	-0.361	00000	0.361	0.721	1.082	1.443	244		7000	177.50	195.0-	2000	0.361	9,721	1.082	1.443	-1.44G	-1.082	-0,721	-0.361	0.361	0.721	1,082	1.443	-1.443	-1.082	-0.721	-0.361	000.0	0.361		• • • • • • • • • • • • • • • • • • • •	1.082	1.443
GAGE		8	m	•	'n	•	^	œ	•	7	~~	m	~	10	•		. or	•		٦ ،	,	ŋ ·	+ u	n ·	•0	~ (00	•	•	~	m	•	9	7	ස	۰		2	1 147	4	· (c) ~	, ,	٠ (י פנ	٥.
STANDOFF DISTANCE	0.436	0.436	0.436	0.436	0.436	0.436	0.436	4	•	•	0.436	٣.	0.436	•	•		0.436	474	75.0	٠	1000	011	•	٠	0.436		٠	C. 435	٥,582	0.582	3.582	0.582	0.582	0.582						0.582	•	•	•	•	282.0	•
CHARGE LE IGHT (NG)	0.222	0.222	0.222	0.222	6.322	0.332	0.222	0.222	0.222	0.222	0.272	0.222	60	0.272	0.222	\$ 223	0,222	6.72	171.		7000	7:55	0.722	7.7.7	0.222	0.137	0.222	0.222	0.222	0.222	0.222	0.222	9.225	0.252	0.222	5000	6.223			۲,	7.00	100	150	1 6		
TEST	281	187	281	281	182	261	281	182	182	160	291	291	291	291	160	291	166	100	101	101	707	105	301	100	301	301	30I	301	Į,	ផ្ល	25.1	25.7	.7.7	157	135	25.	26.7	1 6) (1) (1) (1)	74.J	1 70	2 4 5	, .	9 .		20.1

SUMMARY OF HORIZONTAL ARRAY TESTS

TIME OF ARRIVAL (MS)	0.611	0.365	•	0.343	٠	0.347	•	•	0.629	0.732	0.420	0.378	•		0.393	•	•		•	0.442		٠	0.000	•	0.372	•	0.7:7	0.722	0.470	6()	0.0.0	0.000	0.471	(3.0.5)	1. Sec. 10	5.672	0.712	0.446	0.355	0.407	0.372	0.000	00000	•
POSITIVE DURATION (HS)	0.720	0.365	0.186	0.246	0,126	0.233	980.0	0.357	0.505	0.441	0.515	0.171	0.365	0000	960.0	0.056	0.518	0.444	0.345	0.513	0.147	000.0	0.00	000.0	0.000	0.415	0.367	0.444	0.504	000.0	G. 505	0, 0, 0	0.144	0000.0	6.401	0.557	0.783	0.351	0.153	00000	0.133	0.000	000.0	0,820
POSITIVE IMPULSE (PA-S)	196.8	702.7	357.1	878	0.0	711.8	345.5	428.2	254.5	135.8	440.6	304.2	797.8	1019.5	455.2	123.5	250.6	146.9	161.9	371.6	317.2	0.0	0.0	0.0	186.8	355.0	223.2	126.9	286.1	0.0	0.0	0.0	5530.8	0.0	342.1	20545	131.9	144.8	278.5	784.6	396.6	0.0	0.0	•
	1558.1	0.0	9170.6	18367.9	12013.0	18750.8	10826.5	5950.8	2193.2	971.6	2321.5	1126.1	13951.8	7312.3	8213.7	5014.4	3785.0	1370.8	1338.9	4667.6	4880.1	0.0	0.0	0.0	3718.3	3895.3	1838.8	1230.7	4695.1	0.0	0.0		55514.8	0.0	45:7.4	1409.0	1243.1	5095.9	6353.4	12512.0	6714.9	0.0	0.0	
	0.724	0.724	0.724	0.724	•	0.724		0.724	0.724	0.724	9.724			0.724	0.724	0.724	72	0.724	0.724	0.724	6.724	0.724	0.724	6.724	0.724	0.724	0.724	0.724	0.724	0.724	40.0	0.724			サルバ・0	0.724	0.774	0.724	0.724		0.724	0.724	0.724	, E
Ø - X	-1.443	-1.082	-0.721	-0.361	0.000	0.361	0.721	1.082	1.443	-1.443	-1.082	-0.721	-0.361	000.0	0,361	0.721	1.082	1.443	-1.443	-1.082	-0.721	-0.361	0000	0.361	0.721	1.082	1.443	-1.443	-1.082	-0.721	-0.361	0.000	72.0	0.771	1.082	1.443	.1.443	-1.082	-0.723	-0,361	000.0	0.361	1.443	•
GAGE NG	• • • • • • •	~	m	₹	'n	·a	^	Φ	о -		8	le/)	•	'n	•	^	ω	٠		~	М	4	I O	•9	7	0	0	-	7	m	∢:	·~	•	7	ug)	٥		C1	⊢ ;	*	ษา	9	٥	 1
STANDOFF DISTANCE (P)	0.582	•	•	0.582	•		•		•	•	~		0.724	0.724	0.724	0.724				`:		0.724	Ċ	6.724	0.724	0.724	0.724	0.724	0.724	6.1	7	0.724	· .	r .	1	ζ.		.72	١:	۲,	17	5		7.
CHARGE MEIGHT (KG)	0.222	0.222	0.222	0.222	5.223	6.222	N	0.722	6.723	CI	0.222	~	6,222	0.222	0.222	0.222	0.232	0.227	0.222	0.222	0.225	0.223	0.222	0.122	0.222	0.222	0.222	2.122	0.222	0.223	ey (F4 C1 C1 C2		٠:		e 4	•	•			•		•	•
1557	27.1	27.3	27.1	27.1	27.7	27.1	27.3	27.7	27.3	318	MIN	ZIM	RIM	RIE	***	MIN	ZH	NIE	324	32N	32H	324	NCE	304	32N	N (H)	Z M	RES	334	T.O.	333	200	M	7 h)	ż M	· .	,	:4:	(# #	14	3	•1	ア 4 10	0, 61 61

SUMMARY OF HORIZONTAL ARRAY TESTS

) (r) (s)		STRUBULE	SAGE	3948	CHARGE	PEAK	POSITIVE	POSITIVE	TIME OF
, a	FIGHT	DISTANCE	2	LUCATION	SPACING	PRESSURE	IMFOLSE	DURATION	AKKIVAL
,	(PQ)	£		æ,	Ê	(KPA)	(Pr -S)	(MS)	(MS)
d's E	, ,		2	-1.682	0.361	1215.6	144.8	0.517	0.716
d. M			M	-0.721	•	3158.2	99.	, (-)	.46
356		1	4	-0.361	0.361	16588.8	732.9	6.458	0.352
SCP		0.724	មា	•	•	17396.7	٠.	•	٠,
326	•		Νħ	0.341	0.341	6763.8	439.7	ŗ.	0.381
35P	0.222	0.724	7	0.721	0.351	2213.8	156.5	7	0.474
4,5	•		œ	1.632	•	14320.1	2193.8	609.0	0.726
400	•		٥	1.443	•	6958.7	1376.5	839.0	1.156
368		0.724		-1.443	0.361	563.4	111.7	•	1.140
366	•		7	-1.082		1564.2	171.5	0.537	0.691
36.0	•	`	м	-0.721	•	3275.1	285.4	•	0.475
35P		7	•	-0.361	•	11395.5	754.3	0.460	0.353
472			דע	0.000		4		7	ω,
36.6	•	0.724	•	•	0.362	9914.9	701	0.571	0.357
4	•	0.724		•	•	1748.9	137.2	•	0.473
ac.p		7	. 00	1.082	0.361	375	831	0.507	0.712
445		. 25	• •	1.443		100 to 10	106.00	0.697	1.153
170		. 5		-1.447		5,04,0		0.471	1.100
	•	****	٦ ٢		•	7 1761		282	107 T
Y ()	27776	71	V 1	780.1-	•	0,1071	167.0	0.132	•
3.79	•	0.724	- 73	-0.721	9.361	2012.3	•	0.423	0.43/
378		0.724	→	٠	•	13478.6	434.9	0.221	0.360
H/M	5.222	0.724	S	00000	•	14158.4	1135.5	0.427	0.356
378	•	0.72A	9	0.361	0.361	\$290.6	590.2	•	0.362
37P	•	0.724	^	0.721	0.341	2420.0	155.7	0.334	0.472
378		0.724	œ	•	0.361	2057.0	ŝ	0.546	0.702
377	•	0.724	٥	1.443	0.361	9'8'9	141.3	0.611	1.135
410	•	45.40	-4	-1,443	1.082	0.0	0.0	000.0	000.0
₽ 10		0.724	7	-1.082	1.082	0.0	0.0	00000	000.0
410			M	-0.721	1.082	3145.0	410.4	0.581	4
410		0.724	*	-0.361	1.082	3794.0	472.4	0.633	0.473
014	•	0.724	9	0.361	1.032	3764.5	466.2	•	0.478
CT	•		1	•	1.682	2354.0	229.8	0.498	۲.
413	9.222		٠	1.443	1.082	4138.9	300.9	•	.46
614	•			-1.443	1.062	3265.9	_	•	.40
4 0		.72	7	-1.082	1.082	6449.0	365.3	0.347	6.393
004			~	-0.721	1.682	2987.9	375.2	•	0.467
014	Li		4	-0.361	•	671.		•	*
4 □ 4	Li	.72	u \$	0.000	•		13	0.353	6.417
(*)	۲.		~	0.351	•	000	53	•	•
(7		7.		0.721	•			•	12
7		12	oc oc	1.082	082		4		() ()
C : 4	١,	. 73		1.44.	1,080		3	404.0	4
17	1 4				•	•	. Ir		7 7
7 (.1 (•	٦ ٢٠	9 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	7.027	4 6 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	o i) (0 0
***	Ä	:	٧	•	7001	•	7		3

IVE TIME OF ION ARRIVAL (MS)						0.418	669.0	1.062		0.648		0.178					1.028	9 1.043		4 . 0.399	0.172		ia 0.172		0.684		4 0.904		4 0.348	0.163				
POSITIVE DURATION (MS)	0.424	0.417	0.00	0.17	0.123	0.366	9.406	0.273	0.484	0.352	0.332	0.106	000.0	0000	000.0	0.493	0.687	0.419	000.0	0.414	000.0	000.0	0.758	0.543	0.402	0.509	0.604	0.435	0.314	0.171	0.335	0.176	0.349	
POSITIVE IMPULSE (PA-S)	153.8	239.9	0.0	44.1	362.5	341.1	301.1	105.4	204.8	271.0	293.7	334.4	0. 0	0. 0	0.0	354.3	192.9	110.3	0.0	286.8	ဝ ပ	0.0	575.8	575.0	319.2	243.4	144.1	339.7	288.6	292.6	1414.3	368.9	198.2	1
PEAK PRESSURE (KPA)	843.0	1776.8	0.0	958.5	5410.2	2637.6	1980.5	1442.9	1122.7	1923.1	2263.4	10401.1	0.0	2153.6	0.0	2064.6	1116.9	956.1	0.0	3679.4	8407.9	0.0	6116.1	4606.7	2091.4	1383.1	1007.7	2814.3	3662.4	8388.4	49384.3	11259.1	2369.0	
CHARGE SPACING (M)	0.145	0.145	0.145	0.145	0.145	0.145	0.145	0.145	0.145	0.145	0.145	6.145	0.145	0.145	0.145	0.145	0.145	0.145	0.145	0.145	0.145	0.145	0.145	0.145	0.145	0.145	0.145	0.145	0.145	0.145	0.145	0.145	0.145	
GAGE LOCATION (H)		-1.082	-0.721	-0.361	0.361	0.721	:.082	1.443	-1.443	-1.682	-0.721	-0.361	0.000	0.361	0.721	1.082	1.443	-1.443	-1.082	-0.721	-0.361	0.000	6.361	0.721	1.082	1.443	-1.443	-1.082	-0.721	-0.361	000.0	0.361	0.721	
GAGE	1	8	m	4	•	7	œ	0	74	7	17	4	'n	9	^	œ	۰	-	7	۳۱	4	ın	٥	7	c o	D -	-	~	m	*	I O	•	7	
STANDDFF BISTANCE (A)	0.442	0.442	44.	0.442	44.	44.	4	0.442	7	• •	4	0.442	0.442	۲.	₹.	0.442	0.442	7	0.442	0.442	44.	*	44.	0.442	44	0.442	7	4	0.442	7	7	4	0.442	
CHARGE WEIGH! (KG)	0.222	6.222	0.222	0.222	0.222	0.222	0.222	0.222	0.222	0.222	0.222	0.222	0.033	5.275	0.222	0.222	5000	0.03	2000	5000	et (1)	9.222	7.222	Code V	6 58.7	0.225	0.000	10 C	0.120	0.222	6000	0.222	•	
TEST	191	191	198	198	198	19#	198	19K	23M	234	HE,	1.3h	13.3K	10 M	XI.PI	北門門	X. Fri	24H	248	Zita	MAC	1 × C1	E.	2 14	64 4.	244	***	7: · · · · · · · · · · · · · · · · · · ·	*	447	I. of	***	447	

TABLE A.2 ENGLISH UNIT SUMMARY

SUMMARY OF SINGLE CHARGE TEST DATA

PEAK POSITIVE POSITIVE TINE OF PRESSURE IMPULSE DUKATION ARRIVAL (PSI) (PSI-MS) (MS)		12.6 0.437	0.379	666.7 47.6 0.203 0.384	90.6 0.236	144.3 0.000	2991.7 36.5 0.000 0.197	33.8 0.000	24.8 0.000	17.9	0.427	20.2 0.432	0.192	1304.5 95.4 0.357 0.181	1980.1 160.6 0.129 0.106	3046.7 59.1 0.101 0.186		16.5 0.303	79.9 6.0 7.487 1.073	10.7 0.351	277.0 21.2 0.393 0.660	580.7 46.5 0.277 0.332	96.4 0.246	104.2 0.113	2475.1 116.9 0.180 0.173	39.6 0.211	26.4 0.418	000.0		54.9 0.378	145.0	0.216	398.9 0.260	214.1 0.309	61.9 0.203	673.2 65.7 0.375 0.527	27.7 0.484	241.6 34.0 0.432 0.738	57.2 0.320	99.5	218.1 0.250	291.1 0.212	121.4 0.178
CHARGE SPACING (IN)		0.000	00000	000.0	0.000	00000	0.000	000.0	00000	000.0	000.0	000.0	000.0	0.00	00000	0000	000.0	0000	00000	000.0	000.0	0.000	000.0	00000	000.0	0000	000.0	000.0	00000	00000	000.0	000.0	000.0	00000	0.000	00000	00000	0000	0000	000.0	00000	00000	000.0
GAGE LOCATION (IN)		-56.800	-42.600	-28.400	-14.200	0.00	14.200	29.400	42.600	26.800	-56.800	-42.600	-28.400	-14.200	00000	14.200	28.400	42.600	26.800	-56.800	-42,600	-28.400	-14.200	0000	14.200	28.400	42.600	26.800	-56.800	-42.600	-28.400	-14,200	00000	14.200	28.400	42.600	56.800	-56.800	-42.600	-28.400	-14.200	14.200	28.400
CAGE NO			7	M	4	ĸ	•	7	60	٥	-	7	m	4	v	9	7	80	٥	-	7	м	4	Ŋ	•	7	60	0-	-	~	ы	4	Ŋ	•	7	00	٥.	-4	2	ניו ו	•	. 4	^
STANDOFF DISTANCE (IN)	11 11 11 11 11 11 11 11 11 11 11 11 11	17 20	17.20	17.20	17.20		٠		7	Ġ	•	,	•	•	•	17.20		17.20	7	•		•				•	1		ท่	'n	ท่า	25,70	'n	25,70	ij	25.70	'n	25.70	L.	้ห	10		7
CHARGE UEIGHT (LBS)	11 11 11 11 11 11 11 11 11 11 11 11 11	1.430	1.430	4	1.430	4	4	4	4	4	1.430	4	1.430	1.430	4	1.430	1.430	1.430	4	1.430	1.430	4	1.430	4	1.430	4	4	1.430	5.050	•	•	•	٠	5.050	0.000	5.050	0	5.050	•	0	•	0.5	2
TEST	1	18	18	19	1.4	₹.		14	18		13 A	2A	2A	2 A	2₽	2₩	2 A	2₽	2₽	34	34	34	34	34	34	Ą	34	3₽	20B	20B	20B	20B	208	208	208	208	208	21B	21.0	87.7	218	210	 218

SUMMARY OF SINGLE CHARGE TEST DATA

TIME OF AKRIVAL (MS)	0.752	0.503	0.314	961.0	0.183	0.320	0.497	0.744	0.982	0.530	0.319	0.146	0.086	0.154	0.332	0.615	0.000	0.982	0.590	0.328	0.149	0.075	0.140	0.352	0.620	1.023	1.010	0.411	0.331	0.158	0.125	0.145	0.332	0.611	0.00	1.211	0.781	0.473	0.270	0.276	0.494	0.711	1.214	000.0
POSITIVE DURATION (HS)	0.344	0.315	0.459	0.225	0.240	0.233	0.469	0.731	0.356	0.448	0.295	0.196	0.211	0.162	0.187	0.581	000.0	0.384	0.439	0.312	0.209	0.295	0.233	0.785	0.518	1.863	0.335	0.505	0.372	0.142	0.336	0.119	0.251	6.456	000-0	0.000	0.436	000.0	9.288	000.0	090.0	0.728		000.0
FOSITIVE IMPULSE (PSI-MB)	31.3	F . 68	139.3	225.4	266.8	161.2	73.3	42.4	12.7	24.5	38.5	109.4	223.3	106.3	31.8	24.6	0.0	16.9	26.2	40.1	80.0	290.6	76.5	45.1	32.6	23.1	16.7	27.0	44. 0	50.3	413.2	81.0	36.2	30.4	0.0	16.3	26.3	50.3	113.6	120.3	42.9	36.6	0	~ 0
PEAK PRESSURE	240.2	501.7	1286.3	4844.4	5141.9	2289.7	8.109	256.8	105.6	173.2	481.0	2091.0	11267.2	2209.1	483.8	211.3	0.0	125.9	284.6	541.7	2220.8	11207.6	3887.9	632.7	255.9	140.9	128.6	257.3	478.8	1281.3	11229.1	2610.8	502.9	279.1	0.0	82.8	232.8	338.0	1753.5	1940.9	443.1	240.9		. 0
CHARGE Spacing (In)	0.000		0000	0000	000	000.0	0.000	•	0000	0000	00000	000.0	0.000	0000	0.000	0.000	00000	0.000	00000	00000	0000	0.000		00000		0000	0.000	000.0	0.000	000.0	000.0	000.0	0.000	0.000	0.00	0.000	0.000	•		00000		000.0		0000
GAGE LOCATION (IN)	-3.4.900	000	-28.400	-14.200	002.4	28.400	42.400	24. BOO	000.47	-42.600	-28.400	-14.200	000.0	14.290	28.400	42.600	56.800	-56.800	-42.600	-28.400	-14.200	000.0	14.200	28.400	42.600	26.800	-56.800	-42.600	-28.400	-14.200	0.000	14.290	28.400	42.600	26.800	-56.800	-42.500	-28.400	-14.200	14.265	20 400	42.400		16.800
GAGE		• (V P	• ◀	•	۸ ۵	. a	0	٠,	• •	ł 145	•	· MI	•		. 00	• •			1 17	•	· 163	9 49		. 00	0	-	8	150	•	ŭ.	•0	٠.,	:10	•	-		M	, 4	•	, ,	\ α	•)
STANDOFF DISTANCE (IN)	26. 70	•	25.70		٠	25.70		07.07	•	•	•	•			,	4	, -	4		7	4	•	•	4	•	4.	4	7	4	4	11.40	₹.	4	4		22,90		,			٠	, 0	٠	22.40
CHARGE WEIGHT (LBS)			000		٠		•	2000	0.000	•	•	•	•	•	1.430	•	1.470	•	•	•	1.430	•	•	4	•	•		•		•	•	•	٠	•	. 4		4	•	4		•	• •	•	1.430
test Id	326	977	228	977	4 6	200	900	977	977	י ני	, r	200	20		25	2	, <u>,</u>	ر د د	, מ ה) c	ج ا) d	, &) () ()	, W	, £	200	Ų.	36	26	26	26) O	0	, o	2 2 5	¥.) i:	•	a (3 6	? !	3 F

SUNMAPY OF SINGLE CHARGE TEST DATA

TIME OF ARRIUAL (MS)	1.231	0.501	0.298	0.210	0.2/2	0.468	0.751	1.148	1.140	0.742	0.419	0.272	0.202	0.274	6.473	0.778	0.251	1.510	1.118	0.813	0.621	0.563	0.623	0.813	1.111	1.489	1.514	1.6%	0.773	0.592	0.553	0.572	6.773	1.035	1.508	1.45,4	1.170	0.000	0.865	0.337	0.870	6.978	1.233	1.494
POSITIVE DURATION (#S)	0.375	0.640	9 1	0.254	0.172	•	•	0.691	0.366	0.414	0.768	0.377	0.166	0.238	0.439	0.449	0.798	0.232	0.575	0.731	0.428	0.152	0.360	0.311	0.525	0.745	0.357	0.433	0.643	6.456	0.137	0.389	0.405	0.642	0.566	0.337	0.424	000.6	909.0	0.271	6.417	0.537	0.649	6
FOSITIVE IMFULSE (PSI-MS)	45.6	36.0	117.7	116.3	9.68	46.9	37.4	22.0	13.5	24.0	30.08	97.2	104.0	115.9	51.4	24.7	18.6	9.1	29.2	44.7	54.3	74.3	37.0	27.8	27.9	28.3	12.0	31.1	29.4	61.5	34.6	48.5	37.5	34.2	26.1	0.0	45.°°	•	93.2	113.7	94.9	48.6		42.1
PEAK PRESSURE (PSI)	285.8	410.8	1701.9	2514.3	2066.6	512.2	5.992	95.4	95.3	175.3	300.8	1973.1	2873.4	1751.1	525.3	218.9	80.7	103.1	188.2	322.1	655.7	0.0	536.9	204.7	191.2	114.3	81.1	183.5	191.8	647.9	709.6	693.8	243.9	137.3	110.9	0.0	242.8	0.0	817.4	1149.8	633.6	378.0	296.6	153.4
CHARGE SPACING CIN)	00000	0.00	0.000	0.00	0.000	•	000.0	00000	0.000	00000	0.000	0.000	0.000	0.000	000.0	000.0	•	000.0	000.0	٠	0.000	00000	0.000	0.000	0.000	000.0	0.000	00000	000.0	0.000	0.000	000.0	0.000	000.0	000.0	000.0	0.000	00000	00000	0000	0000	0000	000.0	00000
GAGE LCCATION (IN)	-42.600	-28.400	-14.200	000.0	14.290	28.400	42.600	56:800	-56.860	-42.600	-28.400	-14,200	00000	14.200		42.600	56.800	-56.800	-42.600	-28.400	-14.200	00000	14.700	28.400	42.400	56.890	-54.800	-42.600	-28.400	-14.200	0.000	14.200	28.400	42.600	26.800	-56.800	-42.600		-14.260	00000	14.200	28.400	42.600	56.800
GAGE NO	2	m	4	L7	40	7	ယ	٥	~1	Ç.	m	4	רט	9	7	60	0	-	2	וייל ו	4	רט	9	7	œ	6	-	7	m	4	<u>ن</u>	•0	7	œ	٥.		2	m	4	ภ	9	7	œ	٥
STANDOFF DISTANCE (IN)		•	22.90	•	•	•	-	22.90	22.90	22.70	22.90	22.90	22.90	22.99	22.90	22.90	1		-		-	41.20	•	•	•	٠	41.20	41.20	•	٠	41.20	٠	•	41.20	41.20	٠	61.50	61.50	61.50	61.50	61.50	1.5		1.5
CHARGE WEIGHT (LBS)	1 430	1.430	1.430	1.430	1.430	1.430	1.430	1.430	4	1.450	4	1.430	1.430	1.430		1.450	1.430	•	4	•	•	1.430	1.430	1.430	1 430	1.430	1.430	1.430	1.430	1.430	1,430	1.4.50	1.430	1.430	1.430	5.650	5.050	•	2,039	•	0	٠	0	
TEST ID	30	20	20	5D	25	50	20	50	9	90	9	63	. Q9	6.0	90	97	90	388	388) K	D 38R	38R	36R	38R	38K	38R	40R	4 0%	4 08	40R	40K	40R	40K	40A	4 0%	395	368	358	375	393	37.5	375	365	395

AKRIUAL (MS)	1.147	807.0	0.365	0.000	0.054	0.114	9.376	0.000	1.145	1.145	0.716	0.384	0.150	0.052	0.161	0.394	0.755	1.229	1.183	0.000	6.338	0.191	0.059	0.145	0.3	1,153	1.247	0.784	0.447	0.210	00000	05:0	6.473	0.818	1.338	1.263	0.833	0.413	0.215	0.208	0.479	0.369	4.224	(000
PUST LICE DURATION (MS)	202.0	0.310	0.402	0.000	0.662	0.160	0.462	0.00	0.433	0.358	0.264	0.299	0.160	0.213	980.0	0.469	0.917	0.440	0.550	000.0	0.276	0.207	0.098	0.152	0.293	0.531	0.291	0.421	0.756	6.174	0000	0.170	0.649	0.518	0.450	0.330	0.488	0.454	0.157	0.174	0.351	0.562	0.565	0000
PUSITION IMPULSE (FSI-MS)	11.9	16.2	0.0	40.1	0.0	0.0	34.2	0.0	15.9	17.8	20.0	31.7	55.2	491.5	42.5	34.1	42.6	17.3	16.2	0.0	39.7	0.0	129.2	0.09	34.0	19.8	o. 0	22.0	31.8	57.3	0.0	80.9	₽0.0	32.0	13.0	11.0	24.4	32.1	76.1	42.0	27.3	35.9	17.7	
PEAK PRESSURE (PSI)	90.5	166.5	197.4	0.0	7500.7	819.6	271.8	0.0	101.1	78.3	150.3	414.4	1036.3	5833.1	1195.3	223.8	151.7	100.7	95.7	0.0	305.9	0.0	4487.0	1451.4	282.5	0.0	40.7	157.9	289.7	1328.5	٠. ٥	1655.0	222.0	146.5	83.3	73.2	133.8	231.3	1636.1	0.0	192.6	143.9	77.2	7.57
CHARSE SPACING (IN)	0.000	0.000	000.0	0.000	0000	0.000	0000	0000	00000	000.0	00000	0000	00000	0.000	00000	0000	000.0	0.000	000.0	0.00	0000	0000	0000	000.0	0.000	000.0	0.000	0.000	0000	000.0	0.000	0.000	000.0	0.00	000.0	0.000	000.0	٥٠٥٥٠	0.000	0.000	000.0	000.0	0000	
646E LOCATION (IN)	-56.800	-42.600	-28.400	-14.200	0.000	14.200	28.400	42.600	56.800	-56.800	-42.600	-28.400	-14.200	00000	14.200	28.400	42.60C	56.800	-56.800	-42.500	-28.400	-14.200	000.0	14.200	28.400	26.800	-56.800	-42.600	-28.400	-14.200	000.0	14.200	28.400	42.600	26.800	-56.800	-42.600	-28.460	-14.200	14.200	28.400	42.600	54.800	200.00
GAGE	 	7	m	∢	v	•	7	00	•	-	7	m	4	רט	9	7	60	6		7	ю	•	רט	9	7	٥		7	173	4	เว	9	7	œ	٥	-	7	6-1	4	•9	^	80	0	
STANDOFF DISTANCE (IN)	4	*	11.40		11.40	11.40	11.40	11.40	4	11.40	4	11.40	11.40	11.40	11.40	11.40	11.40	11.40	11.40	11.40	11.40	11.40	11.40	11.40	11.40	Ξ.		'n		•	Ķ	•	ζ.	٠	ĸ	17.20	٠	7	•	•		1	_	٠
CHARGE WEIUHT (LBS)		•	0.490	٠	4	0.490	0.490	0.490	4	0.490	•	0.490	•	0.490	0.490	6.490	0.490	•	•	•	0.+30	0.480	0.490	0.430	0.480	•	•	0.490	•	0.470	•	•	0.400	0.430	•	0.400	0.430			•				0.440
1557	16E	16E	16E	16E	16E	16E	16E	16E	162	17E	17E	17E	1.7E	17E	17E	17E	17E	17E	18E	18E	18E	18E	18E	186	13E	18E	13F	13F	13F	135	13F	13F	13F	13F	13F	14F	14F	14	1.4F	146	1 T	4	1 4 5	141

SUMMARY OF GROUPED ARRAY TESTS

TIME OF ARRIVAL (MS)	0.041	0.216	0.718	0.427	908.0	1.284	1.435	0.992	0.594	0.325	0.172	0.307	0.575	0.753	1.420	1.452	000.0	0.578	0.307	0.176	0.233	0.665	C.795	1.433	1.430	0.995	0.582	0.714	0.325	6.533	0.984	1.418
POSITIVE PURATION (MS)	0.350	0.078	0.091	0.351	0.421	1.484	0.452	0.972	0.492	000.0	0.232	0.273	0.466	0.790	0.661	0.460	000.0	0.406	0.173	000.0	0.295	0.400	0.384	0.457	0.177	0.316	0.187	0.377	0.231	0.251	0.497	0.548
PGSITIVE IMFULSE (FSI-MS)	18.0	41.5	47.2	29.7	32.0	13.8	14.0	41.0	32.3	0.0	115.7	54.6	32.6	43.4	14.6	10.2	0.0	30.5	80.7	6.0	61.4	35.3	29.3	17.8	19.4	15.3	19.0	74.4	46.2	27.6	42.0	29.9
PEAK PRESSURE (PSI)	157.7	1363.5	1521.1	249.3	136.1	89.2	71.4	117.9	191.8	801.6	2521.0	972.3	1/2.2	127.7	89.3	105.0	0.0	182.7	861.1	0.0	1287.2	292.5	101.1	109.6	100.4	196.2	215.4	872.3	1274.1	206.6	180.4	93.9
CHARGE SPACING (IN)	0.000	000.0	00000	00000	000.0	0.000	000.0	0000	00000	00000	000.0	00000	0.000	0.000	0.000	00000	000.0	0.000	00000	0.000	000.0	0.000	0.000	00000	0000	00000	00000	00000	000.0	0.000	0.000	00000
GAGE LOCATION (IN)	: 42.600	-28.400	14.200	28.400	42.600	26.800	-56.800	-42.600	-28.400	-14.200	00000	14.200	28.400	42.600	56.800	-56.800	-42,600	-28.400	-14.200	0.000	14.200	28.400	42.600	56.300	-56.200	-42.609	-29,400	-14.200	14.200	28.400	42.600	26.800
GAGE NO	2	ი ◀	۰ ۰	7	80	c.	~ 1	Ŋ	(4)	4	ĸ	•0	7	œ	٥	-4	7	m	4	ษา	9	۲,	80	•	-	2	м	4	9	7	00	٥
STANDOFF DISTANCE (IN)	17.20	17.20	17.20	17,20	17.20	:7.20	22.92	22.92	22.32	22.92	22.92	22.92	22.92	22.92	22.92	22.92	22.92	22.92	22.92	22.92	22.92	22.32	22.92	22.92	22.92	22.92	22.92	22.92	22.92	22.92	22.92	22.92
CHARGE WEISHT (LBS)	0.490	0.470	0.490	0.490	0.470	0.490	0.490	0.490	0.490	6.490	0.140	0.490	0.490	0.430	0.490	0.430	0.430	0.430	0.430	0.430	0.490	0.490	0.430	0.490	0.430	0.4%	0.490	0.490	0.4.0	0.490	0.496	0.490
TEST	15F	101	L LL 10 10 10 10 10 10 10 10 10 10 10 10 10 1	15F	15F	15F	106	106	106	106	106	106	106	106	106	116	116	116	116	116	116	116	116	116	126	126	126	12.0	126	126	126	126

(TM) (FSI) (FSI)		STANDOFF	GAGE	GAGE LOCATION	CHARGE	FEAK PRESSURE	POSITIVE IMPULSE	POSITIVE DURATION	TIME OF ARKIVAL
40 1 25,800 5,700 122,3 22,3 0,424 40 2 -42,460 5,700 139,0 6,4 0,401 40 4 -14,200 5,700 139,0 6,4 0,401 40 4 1,200 5,700 139,0 6,4 0,173 40 4 1,200 5,700 139,0 5,20 0,173 40 8 4,2600 5,700 287,3 49,3 0,135 40 9 5,6800 5,700 209,3 15,3 0,404 40 1 2,26,400 5,700 209,3 39,3 0,404 40 4 1,4200 5,700 328,3 48,5 0,434 40 4 1,4200 5,700 312,3 48,5 0,434 40 4 2,400 5,700 312,3 48,5 0,434 40 4 2,400 5,700 31,4 31,4 <	D	î		(IN)	(IN)	(FSI)	(PSI-MS)	(MS)	(#3)
2 -42.460 5.700 257.7 34.8 0.417 4 -14.200 5.700 139.0 6.4 0.000 4 -14.200 5.700 139.0 6.4 0.123 5 28.400 5.700 284.7 5.26 0.123 9 5.6800 5.700 287.3 43.7 0.406 1 -5.6800 5.700 289.3 43.7 0.406 1 -5.6800 5.700 289.3 43.7 0.406 2 -42.600 5.700 278.9 43.7 0.406 3 -42.600 5.700 150.8 0.406 0.406 4 -14.200 5.700 150.9 0.0 0.006 5 4.600 5.700 150.0 0.0 0.0 6 14.200 5.700 150.0 0.0 0.0 7 28.400 5.700 150.0 0.0 0.0 8 14.200	17	.40	 	-56.800	5.700	122.3	22.3	0.424	1.029
3 -28,400 5,700 0.0 0.0 0.00 4 14,200 5,700 139.0 6.4 0.123 5 14,200 5,700 282.6 0.123 6 42,600 5,700 287.3 43.7 0.404 9 56,800 5,700 287.3 43.7 0.404 1 -26,800 5,700 209.3 15.3 0.434 2 -42,600 5,700 209.3 15.3 0.434 2 -42,600 5,700 278.3 42.6 0.372 5 0.00 5,700 278.4 0.0 0.0 6 14,200 5,700 29.4 51.4 0.04 7 28,400 5,700 162.0 0.0 0.0 8 42,600 5,700 162.0 0.0 0.0 9 5,700 5,700 162.0 0.0 0.0 1 14,200 5,700 16.0 <td></td> <td>.40</td> <td>8</td> <td>-42,690</td> <td>5.700</td> <td>257.7</td> <td>34.8</td> <td>0.417</td> <td>699.0</td>		.40	8	-42,690	5.700	257.7	34.8	0.417	699.0
4 -14.200 5.700 139.0 6.4 0.177 5 12.200 5.700 382.4 49.5 0.354 6 42.600 5.700 287.3 43.7 0.404 9 56.800 5.700 287.3 15.3 0.434 1 -56.800 5.700 278.9 39.3 0.434 2 -42.600 5.700 328.3 43.5 0.434 2 -42.600 5.700 328.3 42.6 0.135 5 14.200 5.700 1508.4 48.5 0.135 6 14.200 5.700 124.2 0.0 0.00 7 28.400 5.700 124.2 16.0 0.00 8 7.26.800 5.700 124.2 16.0 0.00 9 5.700 5.700 124.2 16.0 0.00 1 -56.800 5.700 14.4 0.0 0.0 2 14.2.600		40	м	-28.400	5.700	0.0	0.0	000.0	0.000
6 14,200 5,700 784.7 52.6 0.123 7 28,400 5,700 287.3 49.5 0.464 9 42,600 5,700 287.3 43.7 0.464 1 -56,800 5,700 209.3 15.3 0.273 1 -56,800 5,700 209.3 43.7 0.444 2 -42,600 5,700 1508.6 0.0 0.0 4 -14,200 5,700 1508.6 0.0 0.0 5 0,000 5,700 150.6 0.0 0.0 6 14,200 5,700 162.0 0.0 0.0 6 14,200 5,700 162.0 0.0 0.0 7 28,400 5,700 162.0 0.0 0.0 8 -26,800 5,700 139.5 0.0 0.0 9 -28,400 5,700 140.2 0.0 0.0 1 -28,800 5,700 </td <td></td> <td>4</td> <td>*</td> <td>-14.200</td> <td>5.700</td> <td>139.0</td> <td>6.4</td> <td>0.177</td> <td>0.162</td>		4	*	-14.200	5.700	139.0	6.4	0.177	0.162
7 28,400 5,700 282,6 49.5 0.364 8 42,600 5,700 287,3 43.7 0.364 9 56,800 5,700 209,3 15.3 0.273 1 -6,800 5,700 208,3 15.3 0.273 2 -28,400 5,700 15.8 42.6 0.332 4 -14,200 5,700 16.9 0.0 0.03 5 14,200 5,700 16.0 0.0 0.0 6 14,200 5,700 16.0 0.0 0.0 7 28,400 5,700 16.0 0.0 0.0 9 5,680 5,700 124,2 28,0 0.0 0.0 1 -56,800 5,700 124,2 41,6 0.0 0.0 2 -4,600 5,700 124,2 41,6 0.0 0.0 3 -4,200 5,700 146,2 0.0 0.0 0.0		4	•	14.200	5.700	784.7	52.6	.0.123	0.175
8 42.600 5.700 287.3 43.7 0.406 9 5.6800 5.700 209.3 15.3 0.404 1 -56.800 5.700 209.3 29.7 0.434 2 -42.600 5.700 328.3 48.5 0.105 3 -14.200 5.700 1508.6 48.5 0.106 4 -14.200 5.700 0.0 0.0 0.00 7 28.400 5.700 29.4 51.4 0.493 8 42.600 5.700 29.4 51.4 0.493 9 5.6800 5.700 124.2 16.0 0.00 1 -6.800 5.700 124.2 16.0 0.00 2 -42.600 5.700 1219.5 0.0 0.00 3 -42.600 5.700 1219.5 0.0 0.00 4 -14.200 5.700 1219.5 0.0 0.0 5 0.000	17		1	28.400	5.700	382.6	49.5	0.366	0.418
9 56.880 5.700 209.3 15.3 0.273 1 -56.880 5.700 278.9 39.3 0.434 2 -42.680 5.700 278.9 39.3 0.434 4 -14.200 5.700 1508.6 48.5 0.106 5 0.000 5.700 312.3 0.0 0.00 6 14.200 5.700 162.0 0.0 0.00 7 28.400 5.700 124.2 16.0 0.00 8 42.600 5.700 124.2 16.0 0.00 9 5.700 124.2 16.0 0.00 1 -42.600 5.700 124.2 16.0 0.00 2 -42.600 5.700 1219.5 0.0 0.00 4 -14.200 5.700 1219.5 0.0 0.00 5 0.00 5.700 1219.5 0.0 0.00 6 142.60 5.700 <td< td=""><td>17.</td><td>4</td><td>8</td><td>42.600</td><td>5.700</td><td>287.3</td><td>43.7</td><td>904.0</td><td>6.9.0</td></td<>	17.	4	8	42.600	5.700	287.3	43.7	904.0	6.9.0
1 -56.800 5.700 162.8 29.7 0.434 2 -42.600 5.700 328.3 42.6 0.332 3 -28.400 5.700 1508.6 48.5 0.106 5 0.00 0.0 0.0 0.00 0.00 6 1.4.200 5.700 124.2 0.0 0.00 7 28.400 5.700 124.2 16.0 0.00 8 42.600 5.700 124.2 16.0 0.00 1 -56.800 5.700 124.2 16.0 0.00 2 -42.600 5.700 124.2 16.0 0.00 3 -28.400 5.700 1219.5 0.0 0.00 4 -14.200 5.700 1219.5 0.0 0.00 5 0.00 5.700 10.0 0.0 0.00 6 14.200 5.700 146.2 0.0 0.00 5 0.00 5.700<			٥	56.800	5.700	209.3	15.3	0.273	1.003
2 -42.600 5.700 278.9 39.3 0.352 3 -42.600 5.700 1328.3 42.6 0.106 4 -14.200 5.700 15.70 0.0 0.0 5 14.200 5.700 0.0 0.0 0.00 7 28.400 5.700 16.0 0.00 0.00 8 42.600 5.700 162.0 0.0 0.00 1 -56.800 5.700 124.2 16.0 0.049 2 -42.600 5.700 124.2 16.0 0.049 3 -28.400 5.700 1219.5 16.0 0.00 4 -14.200 5.700 1219.5 0.0 0.00 5 0.000 5.700 1219.5 0.0 0.00 5 0.000 5.700 1219.5 0.0 0.00 6 14.200 5.700 1219.5 0.0 0.00 5 0.000 5		4	-	-56.800	5.700	162.8	29.7	0.434	1.041
3 -28.400 5.700 158.6 42.6 0.332 4 -14.200 5.700 1508.6 48.5 0.106 5 0.000 5.700 312.3 0.0 0.00 6 14.200 5.700 29.4 51.4 0.00 7 28.400 5.700 124.2 16.0 0.00 9 5.6.800 5.700 124.2 16.0 0.493 1 -56.800 5.700 124.2 16.0 0.419 2 -42.600 5.700 1219.5 0.0 0.419 3 -28.400 5.700 1219.5 0.0 0.00 5 0.000 5.700 1219.5 0.0 0.010 6 14.200 5.700 468.2 48.3 0.543 7 28.400 5.700 201.3 45.3 0.504 8 42.600 5.700 201.3 45.3 0.504 1 -28.400	17.	4	~	-42.600	5.700	278.9	39.3	0.352	6.649
4 -14.200 5.700 1508.6 48.5 0.106 5 0.000 5.700 0.0 0.0 0.00 7 28.400 5.700 0.0 0.0 0.00 7 28.400 5.700 29.4 51.4 0.00 9 75.800 5.700 162.0 0.00 0.00 1 -56.800 5.700 162.0 0.09 0.00 2 -42.600 5.700 129.5 0.0 0.00 3 -28.400 5.700 129.5 0.0 0.00 4 -14.200 5.700 129.5 0.0 0.00 5 0.000 5.700 129.5 0.0 0.00 6 14.200 5.700 146.2 20.9 0.509 7 28.400 5.700 146.2 20.9 0.00 8 -5.600 5.700 146.2 0.09 0.00 14.200 5.700 128.0	17.	4	m	-28.400	5.700	328.3	42.6	0.332	0.409
5 0.000 5.700 0.0 0.000 6 14.200 5.700 312.3 0.0 0.000 7 28.400 5.700 29.4 51.4 0.493 9 42.600 5.700 162.0 28.0 0.000 1 -56.800 5.700 124.2 16.0 0.0493 2 -42.600 5.700 124.2 16.0 0.0493 3 -28.400 5.700 1219.5 0.0 0.00 5 0.000 5.700 1219.5 0.0 0.00 5 0.000 5.700 1219.5 0.0 0.00 5 0.000 5.700 1219.5 0.0 0.00 6 14.200 5.700 483.5 0.543 0.543 7 28.400 5.700 408.2 49.3 0.509 9 5.700 5.700 41.9 0.171 4 -14.200 5.700 41.9 <	17	4	*	-14.200	5.700	1508.6	48.5	0.106	0.178
6 144.200 5.700 312.3 0.0 0.000 7 28.400 5.700 299.4 51.4 0.00 0.00 9 5.6800 5.700 162.0 281.4 0.000 0.000 2 -42.600 5.700 124.2 16.0 0.0493 3 -28.400 5.700 124.2 16.0 0.0493 4 -14.200 5.700 124.2 16.0 0.0414 5 0.000 5.700 0.0 0.0 0.000 5 0.000 5.700 0.0 0.0 0.000 6 14.200 5.700 30.3 46.3 0.543 7 28.400 5.700 30.3 46.3 0.509 9 5.6800 5.700 30.3 46.3 0.509 1 -56.800 5.700 20.3 42.4 0.402 2 -42.600 5.700 5.700 5.09 6.09 0.09	17.	4	li)	00000	5.700	0.0	0.0	0.000	0.000
7 28.400 5.700 0.0 0.0 0.000 8 42.600 5.700 162.0 299.4 51.4 0.493 9 56.800 5.700 162.0 289.0 0.687 1 -56.800 5.700 162.0 28.0 0.687 2 -42.600 5.700 1219.5 0.0 0.000 3 -28.400 5.700 1219.5 0.0 0.000 5 14.200 5.700 183.5 0.00 0.000 6 14.200 5.700 303.3 46.3 0.53 7 28.400 5.700 40.3 0.509 9 56.800 5.700 40.3 0.402 9 56.800 5.700 40.3 0.509 9 57.00 40.63 40.0 0.00 1 -56.800 5.700 40.24 0.171 4 -14.200 5.700 40.24 0.171	17.		•	14.200	5.700	312.3	0.0	0.0.0	0.167
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1 -56.800 5.700 124.2 16.0 0.419 2 -42.679 5.700 533.6 41.6 0.000 3 -14.200 5.700 1219.5 0.0 0.014 4 -14.200 5.700 187.1 83.5 0.000 5 0.000 5.700 668.2 63.4 0.543 7 28.400 5.700 668.2 63.4 0.543 9 5.700 5.700 46.3 0.402 9 5.700 5.700 46.3 0.402 9 5.700 5.700 46.3 0.402 1 -56.800 5.700 408.2 49.3 0.402 2 -42.600 5.700 408.2 49.3 0.402 3 -28.400 5.700 1216.6 42.4 0.171 4 -14.200 5.700 7126.6 205.1 0.349 5 0.000 5.700 343.6 0.349 6 14.200 5.700 343.6 0.099 <	1	40	0-	26.800	5.700	162.0	28.0	0.687	1.078
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.40 9 56.800 5.700 200.2 32.7 1.136	17	4	60	42.600	5.700	431.9	52.9	0.099	0.460
		4	٥	26.800	5.700	200.2	32.7	1.136	605.0

TIME OF AFFIUAL (PS)	0.499	0.104	0.252	6.184	0.251	0.145	0.259	0.532	0.433	0.245	0.161	925.0	0.159	0.239	0.154	0.2.7	9.4.0	0.450	0.219	0.156	0.227	0.134	6.202	0.141	6.255	0.459	0.442	6. ¥.0	0///0	0.3.4	0. 3/1	0.00.0	ر د : : د د	6.634	6.645	0.3/4	* · · · ·	9.9.4	0.253	63.49	00000	301.0	0.647
FOSITIVE DURATION (MS)	0.708	9000 C	0.372	0.317	0.636	0.186	0.422	1.310	0.318	0.348	0000	0.147	0.154	0.259	0.117	0.241	0.500	1.501	0.328	0.178	0.240	0.117	0.232	0.267	0.326	0.500	1.239	0.446	000.0	6.214	6.306	0.000	0.000	0.594	0.418	0.418	6.110	0.223	0.159	0.40	0.000	616	0.411
POSITIVE IMFULSE (PSI~MS)	0	57.2	166.8	91.3	191.8	65.1	75.0	40.0	21.7	50.3	98.2	149.0	125.0	216.4	4.69	54.8	28.3	24.4	54.3	63.5	140.4	94.1	217.6	77.8	8.37	29.0	17.5	39.9	0.0	95.6	19%.6	0.0	46.7	27.1	0.5%	36.9	5.5	96.3	207.8	208.8	0.0	4 64	25.8
PECAK PRESSURE (FSI)	200.3	576.2	4319.B	2876.0	3205.9	3004.0	9.068	430.4	173.0	1138.3	4340.0	4132.0	2997.0	3256.1	30.30.3	1397.1	302.0	224.3	1543.4	1646.4	1976.6	2752.9	4215.4	2465.4	1221.3	263.8	194.7	9.1.69	0.0	ు. 0	2351.1	0.0	977.0	275.5	214.8	626.6	0.0	2231.3	1681.2	2469.3	0.0	41: 4	246.3
CHARGE SPACING (IN)	28.00	28.50	28.50	28.50	28.50	28,56	28.50	28.50	23.50	28.50	23.50	29.50	28.50	78.50	28.50	28.50	20.50	28.50	28.50	24.50	28.50	28.50	28.50	28.50	28.50	28.50	28.50	28.50	28.50	28.50	28.50	28.50	28.50	28.50	28.50	78.50	28.50	28.50	28.50	28.50	28.50	28.50	28.50
GAGE LOCATION (IN)	-56.300	-28.400	-14.200	0.000	14.200	28.400	42.600	56.300	-56.800	-42.600	-28.400	-14.200	0.000	14.200	28.400	42.600	56.800	-56.800	-42.600	-28.400	-14.200	0.000	14.200	28,400	42.600	56.800	-56.800	-42.100	-28.400	-14.200	14.200	28.400	42.600	56.800	-56.800	-42.600	-28.400	-14.200	000.0	14.200	28.400	42.700	26.800
GAGE NO		νm	4	U7	9	7	8	6	-	(1	М	4	bϽ	9	7	00	6	-	2	м	◀	lD.	9	7	œ	٥	H	7	r)	4	9	7	60	٥	,	2	۳	4	เว	9	7	. α) 6 -
STANDOFF DISTANCE (IN)	7.1	17.16	7.1	7.1	17.16	17.16	17.16	17.16	17.16	7	17.16	17.16	17.16	17.16	17.16	17.16	4	7	Ξ.		**		17.16	17.16	7	17.16	22.92	22.92	22.92	22.92	22.92	22.92	22.92	22.92	22.92	22.52	22.92	22.92	22.42	22.92	22.92	22.62	22.62
CHAKGE WEIGHT (LMS)	•	0.44.0			4	0.430	4	4	0.490	٠	0.430	0.470	0.490	0.490	0.490	0.490	0.470	0.490	4	0.430	0.490	0.430	0.490	•	0.490	0.490	0.490	0.430	4	۲.	0.490	4	4.	•	4	5.430	0.490	43	0.490	4	4	A	0.490
TEST ID	281	761 781	Z9I	291	29I	281	187	281	291	291	291	271	162	291	291	291	162	301	301	351	301	301	301	301	301	301	25,0	25J	25,1	257	25.1	25,7	257	25.3	767	563	25J	263	26J	267	26J	· <	26.1

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SUMMARY OF HORIZONTAL ARRAY TESTS

TIME OF ARRIUAL (MS)	0.716	0.362	'n		₹.	0.726	1.156		0.691	0.475	•	M	•	0.473	0.712	1.153	1.100		٠	٠	0.356	0.362	0.472	0.702	1.136	•	0.0.0	0.463	•	٠	•	•	٠	~	٠	٠	4.	۳.	0.438	0.394	۲.	4	0.396
POSITIVE INJEATION (MS)	0.517	ינו כ לי	•	.38	•	٠	9	٠	0.537	•	0.460	•	0.571	0.377	0.507	0.637	0.471	•	0.400	•	٠	0.284	•	•	0.611	•	•	٠	٠	•	٠	•	•	0.347	•	•	0.358	0.665	•		4.	٣.	0.294
POSITIVE IMPULSE (PSI-MS)	21.0		91.6		22.7	18.	ċ	•		41.4	109.4	4	101.8	19.9	40.9	22.7	13.9	27.4	40.9	63.1	164.7	85.6	22.6	רנו	20.5	0.0	0.0	20°5	œ	\sim	33.3	43.6	٠	53.0	٠	67.6	•	71.5	48.4	4	59.0	38.6	51.0
	176.3	53.5	2523.2	981.0	321.8	2149.5	_	81.7	226.9	475.0	1652.8	2174.1	1438.0	253.7	199.5	84.3	84.6	255.5	291.9	1954.9	2055.0	1347.5	7	298.3	98.4	0.0	0.0	459.0	550.6	546.0	341.4	600.3	473.7	947.3	433.4		•	707.8	357.7	820.9	9.069	462.1	1000.7
CHARGE SPACING (IN)		14.20	•	•	14.20	14.20	٠	14.20	14.20	14.20	14.20	٠	•	14.20		14.20	14.20	14.20	14.20	14.20	14.20	14.20	14.20	14.20	•	42.60	42.60	42.60	42.60	42.60	42.60	42.60	42.60	42.60	42.60	42.60	•	ð	42.60	9	•	42.60	•
GAGE LOCATION (IN)	-42.600	-14.200	00000	14.200	28.400	42.500	56.800	-56.800	42.		-14.200	00000	14.200	28.400	42.600	56.800	-56.800	-42.600	CA	-14.200	0.000	14.200	28.400	42.600	26.800	-56.800	5	-28.400	-14.200	14.200	28.400	26.800	-56.800	•	œ	٠	0000	4	28.400	'n	÷	æ	-42.600
GAGE	2	1 4	· W	••	7	60	6	1	7	ю	4	เก	9	7	œ	Φ.		8	m	•	พ	•	7	œ	۰		7	m	•	9	7	٥		2	m	∢	l)	•0	7	00	٥	7	(1
STANDOFF DISTANCE (IN)	28.50	00 00 00 00 00 00 00 00 00 00 00 00 00	28.50	28.50	28.50	28.50	28.50	28.50	28.50	28.50	28.50	28.50	28.50	28.50	28.50	28.50	28.50	28.50	28.50	28.50	28.50	28.50	28.50	28.50	28.50	28.50	28.50	28.50	28.50	28.50	28.50	28.50	å	æ	å	œ	œ.	ä	28.50	ö	œ	ö	'n
CHARGE UE7GHT (LBS)	1 4.	0.440	*	4	4	4	4.	0.490	4.	4.	4	٠	4.	•	4.	4	0.490	0.490	4	4	4	4	4.	*	4	4	4	۲.	0.450	۲.	4	. 45	. 43	. 47	4	.43	4	.49	0.490	4	4.	0.430	۲.
TEST ID	435 435	3 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	4 c	a. G	300	356	35F	36F	36P	36P	36F	36P	36P	362	3.5F	36F	376	37P	37F	37P	37F	37P	37F	375	378	410	410	4:6	410	410	410	4:0	420	430	420	©1. ₹	420	420	400	0 4 ₹	624	430	435

SUMMARY OF HORIZONTAL ARRAY TESTS

₹	
TIME OF ARRIVAL (MS)	0.000 0.459 0.374 0.456 0.456 0.452
POSITIVE DURATION (MS)	0.000 0.397 0.211 0.628 0.294
POSITIVE IMPULSE (PSI-MS)	0.0 61.0 31.3 73.2 73.2 45.9
PEAK PRESSURE (PSI)	0.0 4.424.5 4.23.4 5.106.9
CHARGE SPACING (IN)	42.60 42.60 42.60 42.60 60 60 60
GAGE LOCATION (IN)	-28.400 -14.200 0.000 14.200 28.400 42.600
GAGE NO	m 4 m 4 m 60 €
STANDOFF DISTANCE (IN)	28.28 28.38 28.38 28.38 28.38
CHARGE WEIGHT (LBS)	000000000000000000000000000000000000000
TEST ID	4 3 0 4 3 0 4 3 0 6 4 0 6 6 4 0 6 6 6 6

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